Multiphysics shape optimization based on a level set mesh evolution framework

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Simplified weakly coupled three-physics setting

 $\min_{\Gamma} J(\Gamma, \boldsymbol{v}(\Gamma), p(\Gamma), T(\Gamma), \boldsymbol{u}(\Gamma)).$



• Incompressible Navier-Stokes equations for (\mathbf{v}, p) in Ω_f

$$-\mathrm{div}(\sigma_f(\boldsymbol{v},\boldsymbol{p})) + \rho \nabla \boldsymbol{v} \, \boldsymbol{v} = \boldsymbol{f}_f \text{ in } \Omega_f$$

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Steady-state convection-diffusion for T_f and T_s in Ω_f and Ω_s : $-\operatorname{div}(k_f \nabla T_f) + \rho \mathbf{v} \cdot \nabla T_f = Q_f$ in Ω_f $-\operatorname{div}(k_s \nabla T_s) = Q_s$ in Ω_s

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Linearized thermoelasticity with fluid-structure interaction for *u* in Ω_s:

$$\begin{aligned} -\operatorname{div}(\sigma_s(\boldsymbol{u},T_s)) &= \boldsymbol{f}_s & \text{in } \Omega_s \\ \sigma_s(\boldsymbol{u},T_s) \cdot \boldsymbol{n} &= \sigma_f(\boldsymbol{v},p) \cdot \boldsymbol{n} & \text{on } \Gamma. \end{aligned}$$

Hadamard's method of boundary variations



$$\begin{split} & \Gamma_{\boldsymbol{\theta}} = (I + \boldsymbol{\theta}) \Gamma, \text{ where } \boldsymbol{\theta} \in W_0^{1,\infty}(\Omega, \mathbb{R}^d), \ ||\boldsymbol{\theta}||_{W^{1,\infty}(\mathbb{R}^d, \mathbb{R}^d)} < 1. \\ & J(\Gamma_{\boldsymbol{\theta}}) = J(\Gamma) + \frac{\mathrm{d}J}{\mathrm{d}\boldsymbol{\theta}}(\boldsymbol{\theta}) + o(\boldsymbol{\theta}), \quad \text{ where } \ \frac{|o(\boldsymbol{\theta})|}{||\boldsymbol{\theta}||_{W^{1,\infty}(\Omega, \mathbb{R}^d)}} \xrightarrow{\boldsymbol{\theta} \to 0} 0, \end{split}$$

For industrial applications, we seek to solve

$$\begin{split} \min_{\Gamma} & J(\Gamma, \boldsymbol{v}(\Gamma), \boldsymbol{p}(\Gamma), \mathcal{T}(\Gamma), \boldsymbol{u}(\Gamma)) \\ \text{s.t.} & g_i(\Gamma, \boldsymbol{v}(\Gamma), \boldsymbol{p}(\Gamma), \mathcal{T}(\Gamma), \boldsymbol{u}(\Gamma)) = 0, \ 1 \leq i \leq p \cdot \\ & h_i(\Gamma, \boldsymbol{v}(\Gamma), \boldsymbol{p}(\Gamma), \mathcal{T}(\Gamma), \boldsymbol{u}(\Gamma)) \leq 0, \ 1 \leq i \leq q \end{split}$$

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- 3. Optimization should handle unfeasible initializations Γ
- 4. No fine tuning of optimization algorithm parameters should be required

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- 2. We implement a single analytical formula for

$$\frac{\mathrm{d}}{\mathrm{d}\Gamma}\left[J(\Gamma,\boldsymbol{v}(\Gamma),\boldsymbol{p}(\Gamma),\mathcal{T}(\Gamma),\boldsymbol{u}(\Gamma)\right]$$

for an arbitrary J based on $\frac{\partial J}{\partial \Gamma}, \dots \frac{\partial J}{\partial u}$.

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for an arbitrary J based on $\frac{\partial J}{\partial \Gamma}, \dots, \frac{\partial J}{\partial \mu}$.

3. We designed our own constrained optimization algorithm

We consider the algorithm proposed by Allaire, Dapogny, Frey (2013):

1. Given a mesh and a moving vector field



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2. A level-set function ϕ associated to $\Omega = \Omega_s \cup \Omega_f$ is computed on the mesh.



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Advection of a level set for Ω on the computational mesh.

$$\partial_t \phi + \boldsymbol{\theta} \cdot \nabla \phi = \mathbf{0}$$



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Breaking the zero isoline of the level set.



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Remeshing adaptively the computational mesh.



For instance, for drag minimization

$$J(\Gamma, \boldsymbol{\nu}(\Gamma)) = \int_{\Omega_f} 2\nu e(\boldsymbol{\nu}) : e(\boldsymbol{\nu}) \mathrm{d}x$$

with $e(\mathbf{v}) = (\nabla \mathbf{v} + \nabla \mathbf{v}^T)/2$.

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$$\frac{\partial J}{\partial \Gamma} \cdot \boldsymbol{\theta} = \int_{\Gamma} 2\nu \boldsymbol{e}(\boldsymbol{v}) : \boldsymbol{e}(\boldsymbol{v}) \boldsymbol{\theta} \cdot \boldsymbol{n} \mathrm{d}\boldsymbol{s}$$

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Then the value of $\frac{d}{d\Gamma}[J(\Gamma, \mathbf{v}(\Gamma))]$ is computed analytically and automatically by solving adjoint states.

$$\begin{split} \frac{\mathrm{d}}{\mathrm{d}\theta} \Big[J(\Gamma_{\theta}, \mathbf{v}(\Gamma_{\theta}), p(\Gamma_{\theta}), T(\Gamma_{\theta}), \mathbf{u}(\Gamma_{\theta})) \Big](\theta) \\ &= \overline{\frac{\partial \mathfrak{J}}{\partial \theta}}(\theta) + \int_{\Gamma} (f_{f} \cdot \mathbf{w} - \sigma_{f}(\mathbf{v}, p) : \nabla \mathbf{w} + \mathbf{n} \cdot \sigma_{f}(\mathbf{w}, q) \nabla \mathbf{v} \cdot \mathbf{n} + \mathbf{n} \cdot \sigma_{f}(\mathbf{v}, p) \nabla \mathbf{w} \cdot \mathbf{n})(\theta \cdot \mathbf{n}) \mathrm{d}s \\ &+ \int_{\Gamma} \Big(k_{s} \nabla T_{s} \cdot \nabla S_{s} - k_{f} \nabla T_{f} \cdot \nabla S_{f} + Q_{f} S_{f} - Q_{s} S_{s} - 2k_{s} \frac{\partial T_{s}}{\partial n} \frac{\partial S_{s}}{\partial n} + 2k_{f} \frac{\partial T_{f}}{\partial n} \frac{\partial S_{f}}{\partial n} \Big) (\theta \cdot \mathbf{n}) \mathrm{d}s \\ &+ \int_{\Gamma} \big(\sigma_{s}(\mathbf{u}, T_{s}) : \nabla \mathbf{r} - \mathbf{f}_{s} \cdot \mathbf{r} - \mathbf{n} \cdot A \mathbf{e}(\mathbf{r}) \nabla \mathbf{u} \cdot \mathbf{n} - \mathbf{n} \cdot \sigma_{s}(\mathbf{u}, T_{s}) \nabla \mathbf{r} \cdot \mathbf{n}) (\theta \cdot \mathbf{n}) \mathrm{d}s \end{split}$$

$$\int_{\Omega_s} Ae(\boldsymbol{r}) : \nabla \boldsymbol{r}' \mathrm{d} \boldsymbol{x} = \frac{\partial \mathfrak{J}}{\partial \hat{\boldsymbol{u}}}(\boldsymbol{r}') \quad \forall \boldsymbol{r}' \in V_{\boldsymbol{u}}(\Gamma) \,.$$

$$\begin{split} \int_{\Omega_{s}} Ae(\boldsymbol{r}) : \nabla \boldsymbol{r}' \, \mathrm{d}\boldsymbol{x} &= \frac{\partial \mathfrak{J}}{\partial \hat{\boldsymbol{u}}}(\boldsymbol{r}') \quad \forall \boldsymbol{r}' \in V_{\boldsymbol{u}}(\Gamma) \, . \\ & \downarrow \\ \\ \int_{\Omega_{s}} k_{s} \nabla S \cdot \nabla S' \, \mathrm{d}\boldsymbol{x} + \int_{\Omega_{f}} (k_{f} \nabla S \cdot \nabla S' + \rho c_{p} S \boldsymbol{v} \cdot \nabla S') \, \mathrm{d}\boldsymbol{x} &= \int_{\Omega_{s}} \alpha \operatorname{div}(\boldsymbol{r}) S' \, \mathrm{d}\boldsymbol{x} + \frac{\partial \mathfrak{J}}{\partial \hat{\boldsymbol{T}}}(S) \quad \forall S' \in V_{T}(\Gamma) \, . \end{split}$$

$$\int_{\Omega_{s}} Ae(\mathbf{r}) : \nabla \mathbf{r}' d\mathbf{x} = \frac{\partial \mathfrak{J}}{\partial \mathbf{u}}(\mathbf{r}') \quad \forall \mathbf{r}' \in V_{u}(\Gamma).$$

$$\downarrow$$

$$\int_{\Omega_{s}} k_{s} \nabla S \cdot \nabla S' d\mathbf{x} + \int_{\Omega_{f}} (k_{f} \nabla S \cdot \nabla S' + \rho c_{p} S \mathbf{v} \cdot \nabla S') d\mathbf{x} = \int_{\Omega_{s}} \alpha \operatorname{div}(\mathbf{r}) S' d\mathbf{x} + \frac{\partial \mathfrak{J}}{\partial \hat{\mathbf{f}}}(S) \quad \forall S' \in V_{T}(\Gamma)$$

$$\downarrow$$

$$\mathbf{w} = \mathbf{r} \text{ on } \Gamma \text{ and } \forall (\mathbf{w}', q') \in V_{v, p}(\Gamma)$$

$$\int_{\Omega_{f}} \left(\sigma_{f}(\mathbf{w}, q) : \nabla \mathbf{w}' + \rho \mathbf{w} \cdot \nabla \mathbf{w}' \cdot \mathbf{v} + \rho \mathbf{w} \cdot \nabla \mathbf{v} \cdot \mathbf{w}' - q' \operatorname{div}(\mathbf{w}) \right) d\mathbf{x} =$$

$$\int_{\Omega_{f}} -\rho c_{p} S \nabla T \cdot \mathbf{w}' d\mathbf{x} + \frac{\partial \mathfrak{J}}{\partial (\mathbf{v}', p')} (\mathbf{w}', q'),$$

$$\min_{\substack{(x_1, x_2) \in \mathbb{R}^2 \\ \text{s.t.}}} J(x_1, x_2) = x_1^2 + (x_2 + 3)^2$$

$$s.t. \begin{cases} h_1(x_1, x_2) = -x_1^2 + x_2 &\leq 0 \\ h_2(x_1, x_2) = -x_1 - x_2 - 2 &\leq 0 \end{cases}$$



All in all, we solve an ODE of the form

$$\dot{x} = -\alpha_J \xi_J(x) - \alpha_C \xi_C(x)$$

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$$\{\xi \in \mathbb{R}^n, Dh_i(x)\xi = 0 \text{ for } i \in I\}$$

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- 3. The subset *I* can determined by solving some dual quadratic optimization subproblem.
- $-\xi_C(x)$ is a Gauss-Newton direction moving the trajectory back onto the feasible set:

$$\mathrm{D}h_i(-\xi_C(x))=-h_i(x).$$



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Volume minimization subject to rigidity constraint

$$\min_{\Omega} \int_{\Omega_s} \mathrm{d}x$$

s.t. $\int_{\Omega_s} Ae(\boldsymbol{u}) : e(\boldsymbol{u}) \mathrm{d}x \leq C$

Volume minimization subject to multiple load rigidity constraints

$$\min_{\Omega} \int_{\Omega_s} dx s.t. \int_{\Omega_s} Ae(\boldsymbol{u}_i) : e(\boldsymbol{u}_i) dx \le C_i, \quad \forall i = 1 \dots 9$$

Lift maximisation subject to drag, volume and center of mass constraint:

$$\max_{\Omega} \int_{\partial\Omega_{f}} \boldsymbol{e}_{y} \cdot \sigma_{f}(\boldsymbol{v}, \boldsymbol{p}) \cdot \boldsymbol{n} dx$$

$$s.t. \begin{cases} \int_{\Omega_{f}} 2\nu \boldsymbol{e}(\boldsymbol{v}) : \boldsymbol{e}(\boldsymbol{v}) dx \leq C_{drag}, \\ \int_{\Omega_{f}} dx = C_{vol}, \\ \int_{\Omega_{f}} \mathbf{x} dx = 0 \end{cases}$$

Heat transfer subject to maximal pressure drop, volume and center of mass constraint:

$$\max_{\Omega} \int_{\partial\Omega_{f,out}} \rho c_p T \mathbf{v} \cdot \mathbf{n} Ds - \int_{\partial\Omega_{f,in}} \rho c_p T \mathbf{v} \cdot \mathbf{n} Ds$$

s.t.
$$\int_{\partial\Omega_{f,out}} p ds - \int_{\partial\Omega_{f,in}} p ds \leq DP_0$$

Heat exchange subject to maximal pressure drop and non penetration constraint:

$$\begin{split} \max_{\Omega} & \int_{\Omega_{f,cold}} \rho c_{p} \mathbf{v} \cdot \nabla T \mathrm{d}x - \int_{\Omega_{f,hot}} \rho c_{p} \mathbf{v} \cdot \nabla T \mathrm{d}x \\ s.t. & \int_{\partial\Omega_{f,out}} p \mathrm{d}s - \int_{\partial\Omega_{f,in}} p \mathrm{d}s \leq \mathrm{DP}_{0}, \\ & d(\Omega_{f,hot}, \Omega_{f,cold}) \geqslant d_{\min} \end{split}$$

Demonstrations on shape optimization test cases

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FEPPON, F., ALLAIRE, G., BORDEU, F., CORTIAL, J., AND DAPOGNY, C. Shape optimization of a coupled thermal fluid-structure problem in a level set mesh evolution framework. HAL preprint hal-01686770 (2018).

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