

Lecture 12: shape optimization with geometric constraints.

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Given a Lipschitz domain Ω , we parameterize deformations of Ω by a continuous vector field θ :

$$\Omega_\theta := (I + \theta)\Omega = \{x + \theta(x) \mid x \in \Omega\}$$

Geometric constraints

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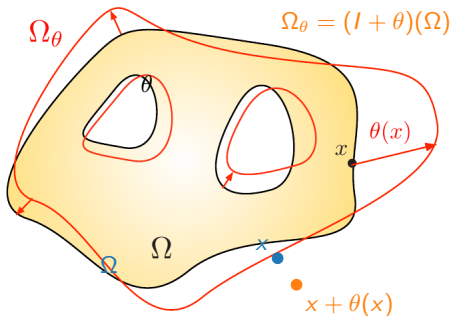


Figure: Deformation of a domain Ω with the method of Hadamard. A small vector field θ is used to deform Ω into $\Omega_\theta = (I + \theta)\Omega$.

Shape/Topology optimization is the mathematical art of generating shapes that best fulfill a proposed objective.

Generically, a design optimization problem arises under the form

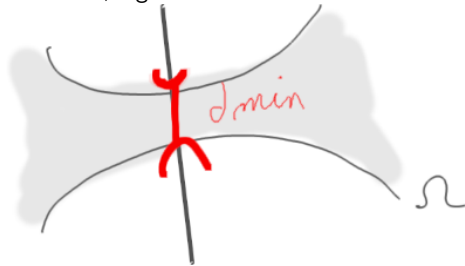
$$\begin{aligned} \min_{\Omega \subset D} \quad & J(\Omega) \\ \text{s.t.} \quad & \begin{cases} G_i(\Omega) = 0, & 1 \leq i \leq p \\ H_j(\Omega) \leq 0, & 1 \leq j \leq q \end{cases} \end{aligned}$$

where

- ▶ Ω is an **open domain** sought to be optimized
- ▶ J is an **objective function** to minimize (corresponding to a measure of the performance)
- ▶ G_i and H_j are respectively p and q **equality and inequality constraints** (corresponding e.g. to industrial specifications to meet)

Shape optimization problems

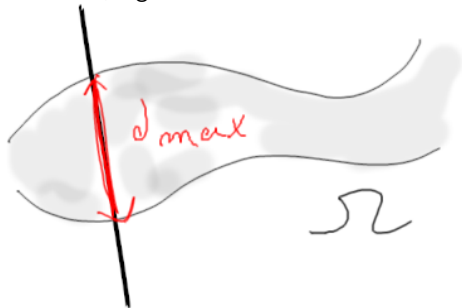
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- ▶ minimum thickness

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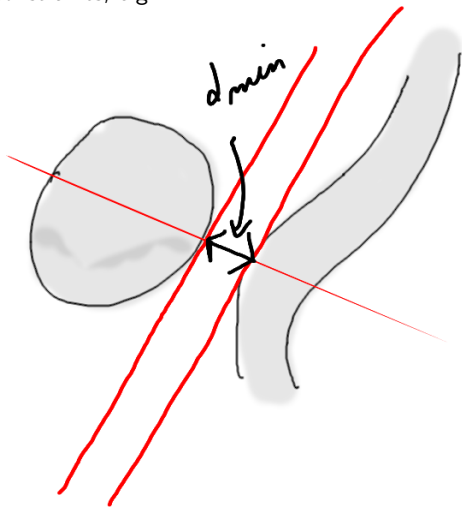


- ▶ minimum thickness
- ▶ maximum thickness

Shape optimization problems

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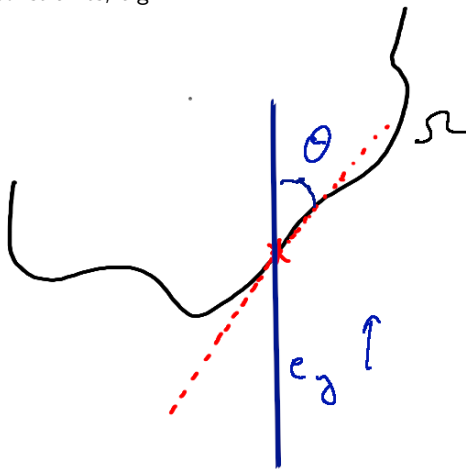
- ▶ minimum thickness
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- ▶ minimum distance between to connected components



Shape optimization problems

Today: how to take into account **geometric** constraints, e.g.:

- ▶ minimum thickness
- ▶ maximum thickness
- ▶ minimum distance between to connected components
- ▶ minimum angle with respect to a direction (overhang)



1. The signed distance function
2. Formulation of geometric constraints
3. Shape derivatives of geometric constraints
4. Numerical examples

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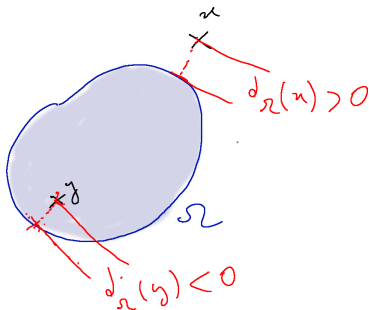
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The signed distance function

Definition 1

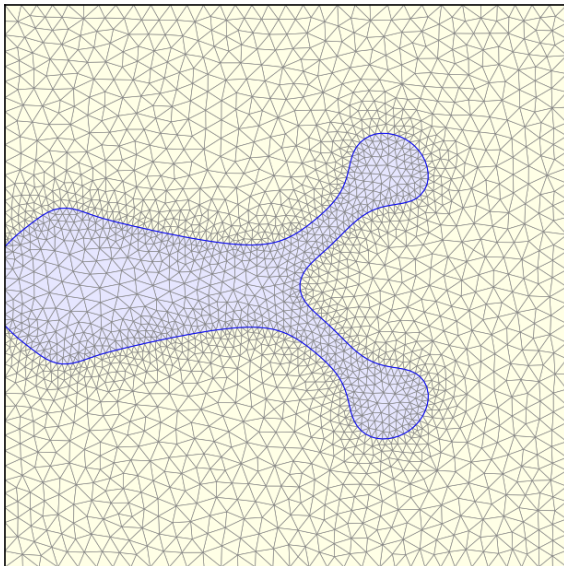
The signed distance function d_Ω to the domain $\Omega \subset D$ is defined by:

$$\forall x \in D, d_\Omega(x) = \begin{cases} -\min_{y \in \partial\Omega} \|y - x\| & \text{if } x \in \Omega, \\ \min_{y \in \partial\Omega} \|y - x\| & \text{if } x \in D \setminus \Omega. \end{cases}$$



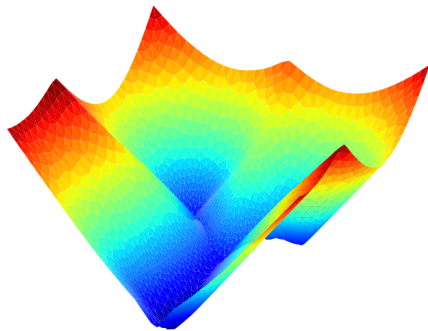
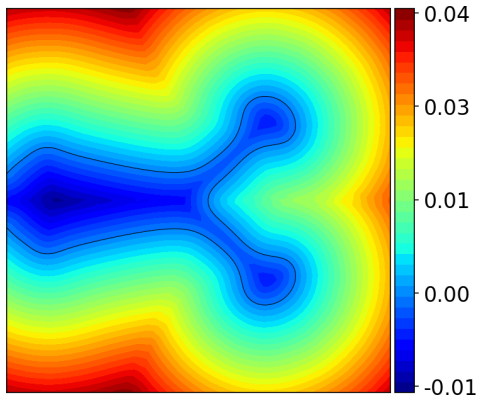
The signed distance function

An example: a meshed subdomain $\Omega \subset D$



The signed distance function

An example: the signed distance function d_{Ω} :



Definition 2 (Skeleton set and projection)

1. The set of points $x \in \mathbb{R}^d$ for which the minimization problem

$$\min_{y \in \partial\Omega} \|x - y\| \tag{1}$$

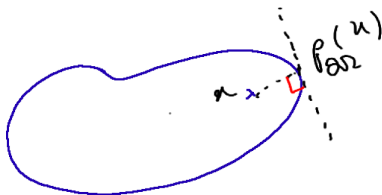
admits several minimizers is called the *skeleton* of Ω and is denoted by Σ .

The signed distance function

Definition 2 (Skeleton set and projection)

2. For any $x \in \mathbb{R}^d \setminus \Sigma$, the unique minimizer of eq. (1) is denoted $p_{\partial\Omega}(x)$ and is called the (orthogonal) *projection* of x onto $\partial\Omega$, in that case it holds

$$\forall x \in \mathbb{R}^d \setminus \Sigma, d_{\Omega}(x) = \begin{cases} -\|x - p_{\partial\Omega}(x)\| & \text{if } x \in \Omega, \\ \|x - p_{\partial\Omega}(x)\| & \text{if } x \notin \Omega. \end{cases}$$

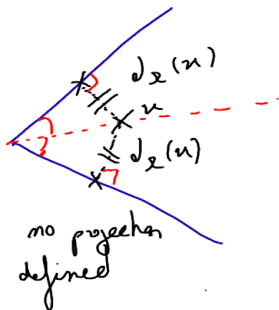


The signed distance function

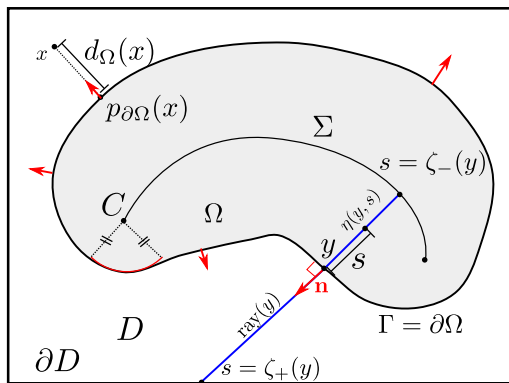
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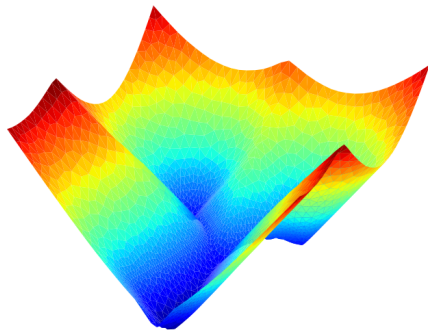
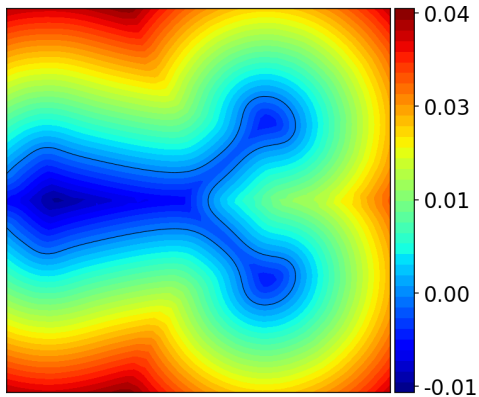
Proposition 1 (Differentiability of d_Ω)

Assume Ω is a C^1 domain with outward normal \mathbf{n} .

- ▶ The signed distance function d_Ω is differentiable at any point $x \in \mathbb{R}^d \setminus \Sigma$, and it is not differentiable on Σ .

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An example: the signed distance function d_{Ω} :



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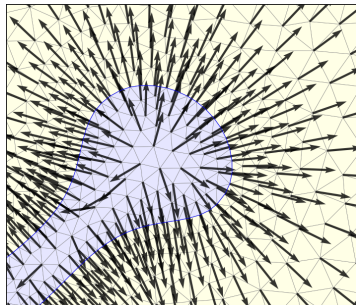
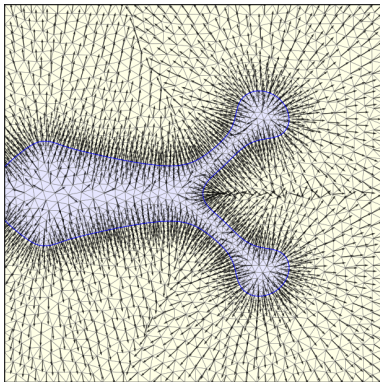
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- ▶ The signed distance function d_Ω is differentiable at any point $x \in \mathbb{R}^d \setminus \Sigma$, and it is not differentiable on Σ .
- ▶ The gradient ∇d_Ω is an extension of the unit normal vector \mathbf{n} to $\partial\Omega$ pointing outward Ω :

$$\forall x \in \mathbb{R}^d \setminus \Sigma, \nabla d_\Omega(x) = \mathbf{n}(p_{\partial\Omega}(x)).$$

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An example: the gradient of the signed distance function ∇d_{Ω} :



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- ▶ In particular, d_Ω solves the so-called "Eikonal" equation:

$$\begin{cases} \|\nabla d_\Omega\| = 1 & \text{in } \mathbb{R}^d \setminus \Sigma, \\ d_\Omega = 0 & \text{on } \partial\Omega. \end{cases}$$

Definition 3

The ray emerging from y is defined to be the one-dimensional segment

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For any $y \in \partial\Omega$, define $\zeta_-(y)$ and $\zeta_+(y)$ the distance at which the ray hits the boundary of D or the skeleton:

$$\forall y \in \partial\Omega, \zeta_+(y) = \sup\{s \geq 0 \mid \{y + t\nabla d_\Omega(y) \mid t \in [0, s]\} \cap (\bar{\Sigma} \cup \partial D) = \emptyset\},$$

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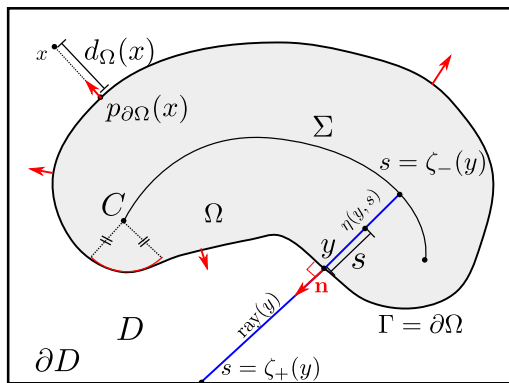
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Then we also have

$$\text{ray}(y) = \{y + sn(y) \mid \zeta_-(y) < s < \zeta_+(y)\}.$$

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Some general principles:

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- ▶ Sometimes, enforcing strictly the constraint might not be desirable because the feasible region becomes tight, or because it may prevent topological changes (such as minimum thickness).

A trade-off can be achieved by **setting the value desired for the objective function as a constraint**, e.g.:

$$\begin{aligned} \min_{\Omega \subset D} \quad & P(\Omega) \\ \text{s.t.} \quad & J(\Omega) \leq 0.9J_{opt} \end{aligned}$$

where J_{opt} would be the optimal value without the constraint.

Formulation of geometric constraints

Maximum thickness

- ▶ Maximum thickness can be formulated as follows:

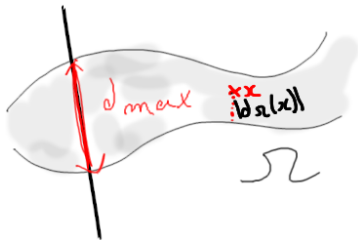
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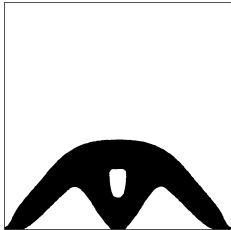
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- ▶ This means taking into account the **averaged constraint**

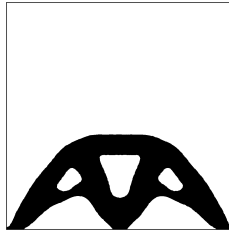
$$P_{\max}(\Omega) \leq d_{\max} \text{ with } P_{\max}(\Omega) := 2 \left(\frac{1}{|\Omega|} \int_{\Omega} |d_{\Omega}|^p dx \right)^{\frac{1}{p}}.$$

Formulation of geometric constraints

Maximum thickness



(a) No maximum thickness constraint



(b) $d_{\max} = 0.07$.

Figure: Maximum thickness constraint for 2D arch.

Formulation of geometric constraints

Minimum thickness

- ▶ Minimum thickness can be modelled by the condition that the shape has a distance greater than $d_{\min}/2$ to its skeleton:

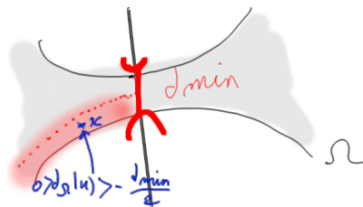
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 3. Enforcing the minimum thickness **at all iterations** would prevent topological changes to occur.
- ▶ It is better to rely on a more flexible formulation

Formulation of geometric constraints

Minimum thickness

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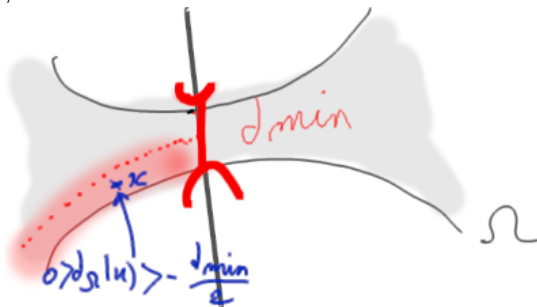
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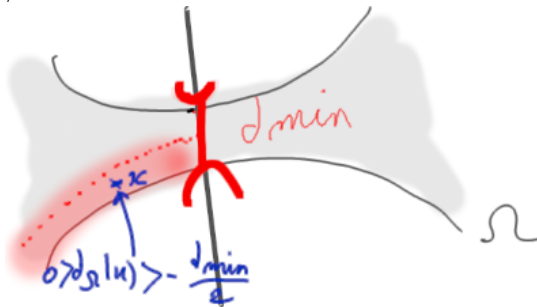
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- ▶ In order to find a good compromise between thickness and the original optimization problem, we use the reformulation

$$\begin{aligned} \min_{\Omega \subset D} \quad & P_{\min}(\Omega) \\ \text{s. t.} \quad & J(\Omega) \leq \alpha J_{opt} \end{aligned}$$

where α is the loss of performance we allow on the objective function due to the minimum thickness requirement

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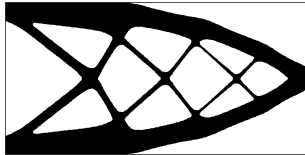
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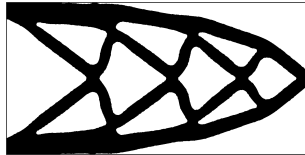
- ▶ the minimization will find shapes with good performances and which satisfy approximately the minimum thickness constraint.

Formulation of geometric constraints

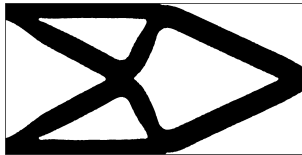
Minimum thickness



(a) No minimum thickness constraint.



(b) $d_{\min} = 0.1$.

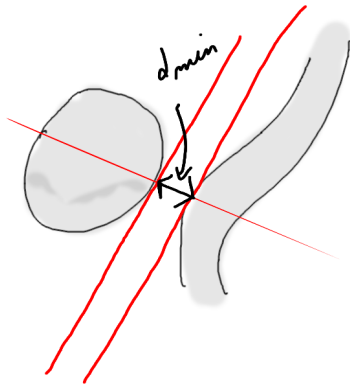


(c) $d_{\min} = 0.2$

Figure: Minimum thickness constraint for 2D cantilever.

Formulation of geometric constraints

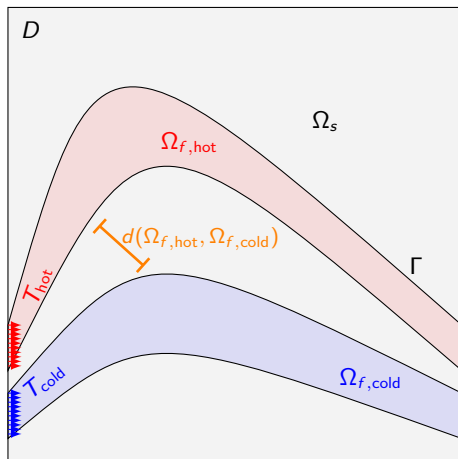
Distance constraint:



Formulation of geometric constraints

Minimum distance constraint

An application: heat-exchangers:



Distance constraint:

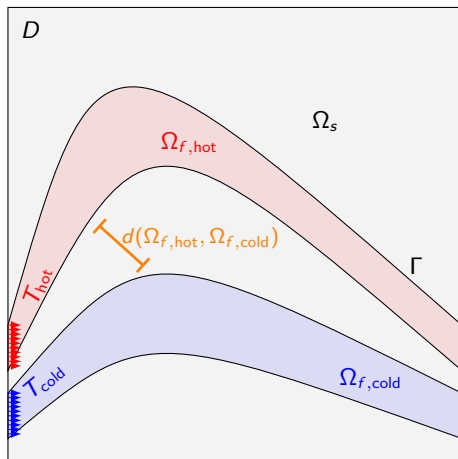
$$d(\Omega_{f,hot}, \Omega_{f,cold}) \geq d_{min}.$$

Figure: Minimum distance constraint for two-fluid heat-exchangers.

Formulation of geometric constraints

Minimum distance constraint

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Distance constraint:

$$d(\Omega_{f,hot}, \Omega_{f,cold}) \geq d_{min}.$$

We enforce it by imposing

$$\forall x \in \Omega_{f,cold}, d_{\Omega_{f,hot}}(x) \geq d_{min},$$

where $d_{\Omega_{f,hot}}$ is the signed distance function to the domain $\Omega_{f,hot}$.

Figure: Minimum distance constraint for two-fluid heat-exchangers.

Formulation of geometric constraints

Minimum distance constraint

$$\forall x \in \Omega_{f,\text{cold}}, d_{\Omega_{f,\text{hot}}}(x) \geq d_{\min},$$

This constraint can be equivalently formulated as

$$\left\| \frac{1}{d_{\Omega_{f,\text{hot}}}} \right\|_{L^\infty(\Omega_{f,\text{cold}})} \leq \frac{1}{d_{\min}} \Leftrightarrow \left\| \frac{1}{d_{\Omega_{f,\text{hot}}}} \right\|_{L^\infty(\Omega_{f,\text{cold}})}^{-1} \geq d_{\min}.$$

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We can approximate it by

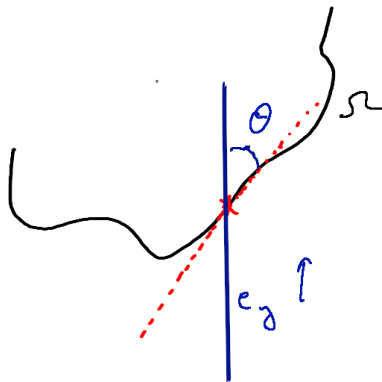
$$Q_{\text{hot} \rightarrow \text{cold}}(\Omega_f) \geq d_{\min}$$

where

$$Q_{\text{hot} \rightarrow \text{cold}}(\Omega_f) := \left(\int_{\Omega_{f,\text{cold}}} \frac{1}{|d_{\Omega_{f,\text{hot}}}|^p} dx \right)^{-\frac{1}{p}}.$$

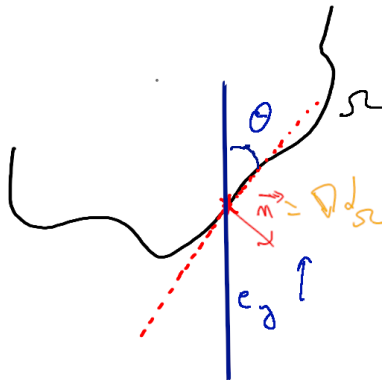
Formulation of geometric constraints

Overhang constraint



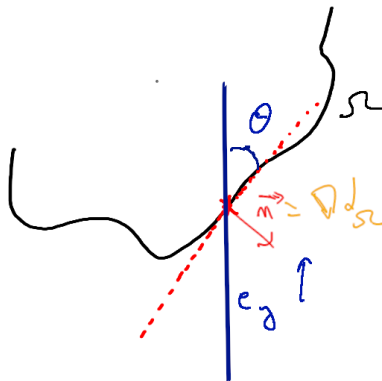
Formulation of geometric constraints

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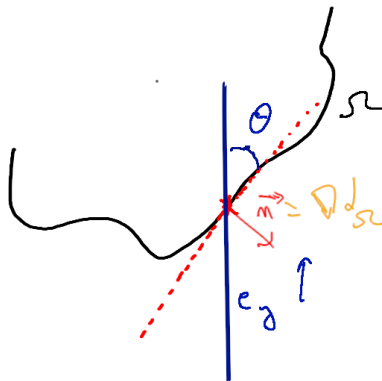
Overhang constraint: the angle θ between the tangent plane and the vertical direction must not be too large, e.g.

$$\theta \leq \beta$$

where β is the maximum angle allowed (e.g. $\beta = \pi/4$).

Formulation of geometric constraints

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Equivalently:

$$\forall y \in \partial\Omega, \mathbf{n}(y) \cdot \mathbf{e}_y = \cos(\pi/2 + \theta) = -\sin(\theta) \geq -\sin(\beta).$$

Formulation of geometric constraints

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$$\forall y \in \partial\Omega, \mathbf{n}(y) \cdot \mathbf{e}_y = \cos(\pi/2 + \theta) = -\sin(\theta) \geq -\sin(\beta).$$

Remembering that $\mathbf{n}(y) = \nabla d_{\Omega}(y)$, we can formulate this in terms of d_{Ω} :

$$\forall y \in \partial\Omega, \nabla d_{\Omega}(y) \cdot \mathbf{e}_y \geq -\sin(\beta).$$

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Since ∇d_{Ω} is an extension of the normal along the rays, we can in fact consider

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This is equivalent to

$$\nabla d_{\Omega} \cdot \mathbf{e}_y + \sin \beta \geq 0,$$

for instance

$$P_{\beta}(\Omega) = 0 \text{ with } P_{\beta}(\Omega) := \int_{\Omega} \min(\nabla d_{\Omega} \cdot \mathbf{e}_y + \sin(\beta), 0)^2 dx.$$

- ▶ Maximum thickness:

$$P_{\max}(\Omega) \leq d_{\max} \text{ with } P_{\max}(\Omega) := 2 \left(\frac{1}{|\Omega|} \int_{\Omega} |d_{\Omega}|^p dx \right)^{\frac{1}{p}}.$$

Formulation of geometric constraints

Recap

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1. The signed distance function
2. Formulation of geometric constraints
3. Shape derivatives of geometric constraints
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All the previous formulations bring into play functionals formulated in terms of the signed distance function d_Ω , e.g.

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In order to compute the shape derivative of $P(\Omega)$, we need to compute the shape derivative $d'_\Omega(\theta)$.

Proposition 3

For any $x \notin \Sigma$, the map $\theta \mapsto d_{(I+\theta)\Omega}(x)$ is Gâteaux-differentiable at θ as an application from $W^{1,\infty}(\mathbb{R}^d, \mathbb{R}^d)$ into \mathbb{R}^d and its derivative reads

$$d'_{\Omega}(\theta)(x) = -\theta(p_{\partial\Omega}(x)) \cdot \mathbf{n}(p_{\partial\Omega}(x)).$$

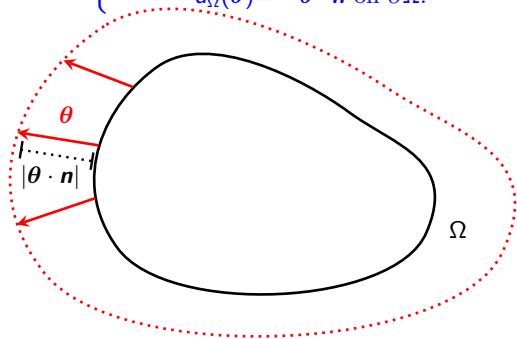
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Equivalently, $d'_\Omega(\theta)$ is characterized by the boundary value problem

$$\begin{cases} \nabla d'_\Omega(\theta) \cdot \nabla d_\Omega = 0 & \text{in } D \setminus \bar{\Sigma} \\ d'_\Omega(\theta) = -\theta \cdot \mathbf{n} & \text{on } \partial\Omega. \end{cases}$$



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The composition with the projection $p_{\partial\Omega}$ is not very easy to implement.

Proposition 4

For any $\theta \in W^{1,\infty}(D, \mathbb{R}^d)$, we have

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 &= \int_{\partial\Omega} u(y) \theta(y) \cdot \mathbf{n}(y) d\sigma(y)
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$$\text{with } u(y) = - \int_{z \in \text{ray}(y)} j'(d_\Omega(z)) \prod_{i=1}^{d-1} (1 + \kappa_i(y) d_\Omega(z)) dz.$$

Shape derivatives of geometric constraints

$$P'(\Omega) = \int_{\partial\Omega} u(y)\boldsymbol{\theta}(y) \cdot \mathbf{n}(y) d\sigma(y) \text{ with } u(y) = - \int_{z \in \text{ray}(y)} j'(d_\Omega(z)) \prod_{i=1}^{d-1} (1 + \kappa_i(y) d_\Omega(z)) dz.$$

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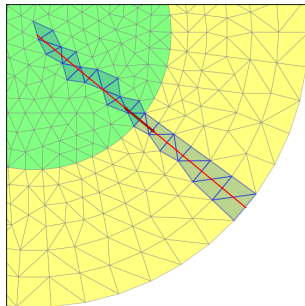
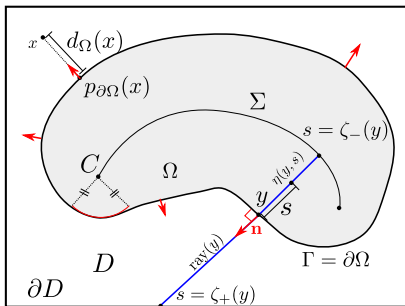
Computing u requires:

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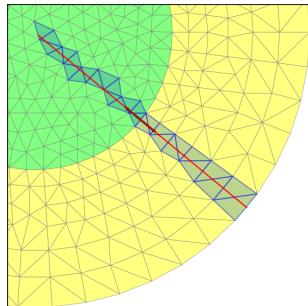
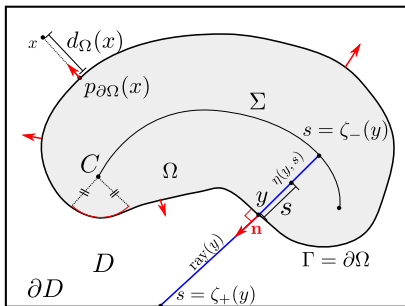


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Computing u requires:

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2. Estimating the principal curvatures $\kappa_i(y)$.

These two operations are quite delicate to implement !

It turns out that it is possible to compute u without integrating along the rays:

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Proposition 5

Let $\hat{u} \in V_\omega$ be the solution to the variational problem

$$\forall v \in V_\omega, \int_{\partial\Omega} \hat{u} v ds + \int_D \omega (\nabla d_\Omega \cdot \nabla \hat{u}) (\nabla d_\Omega \cdot \nabla v) dx = - \int_D j'(d_\Omega) v dx,$$

Then $u(y) = \hat{u}(y)$ for any $y \in \partial\Omega$.

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$\omega > 0$ is a weight that can be chosen rather arbitrarily.

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Then $u(y) = \hat{u}(y)$ for any $y \in \partial\Omega$.

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Sketch of the proof.

Take $v = -d'_\Omega(\theta)$. Since $\nabla v \cdot \nabla d_\Omega = 0$ and $v = \theta \cdot \mathbf{n}$ on $\partial\Omega$, one finds

$$\int_{\partial\Omega} \hat{u} \theta \cdot \mathbf{n} ds = \int_D j'(d_\Omega) d'_\Omega(\theta) dx.$$

whence $\hat{u} = u$ on $\partial\Omega$.



Recap:

- ▶ The shape derivative of a geometric constraint of the form

$$P(\Omega) = \int_D j(d_\Omega(x)) dx$$

reads

$$P'(\Omega)(\theta) = \int_D j'(d_\Omega) d'_\Omega(\theta) dx = \int_{\partial\Omega} u\theta \cdot \mathbf{n} ds.$$

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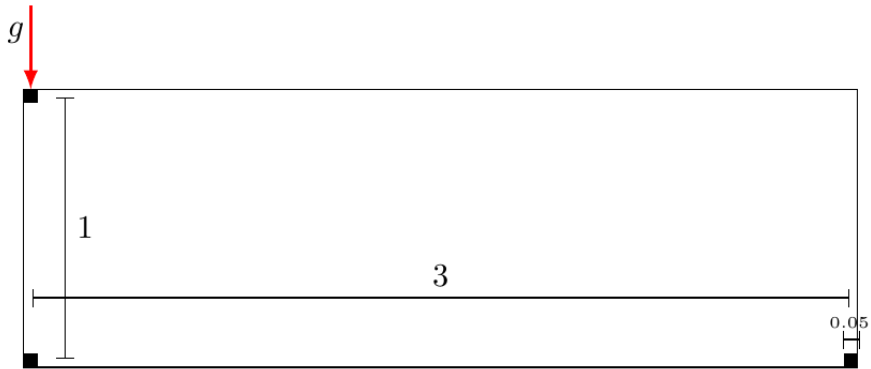
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Numerical examples

Maximum thickness on MBB beam



Numerical examples

Maximum thickness on MBB beam

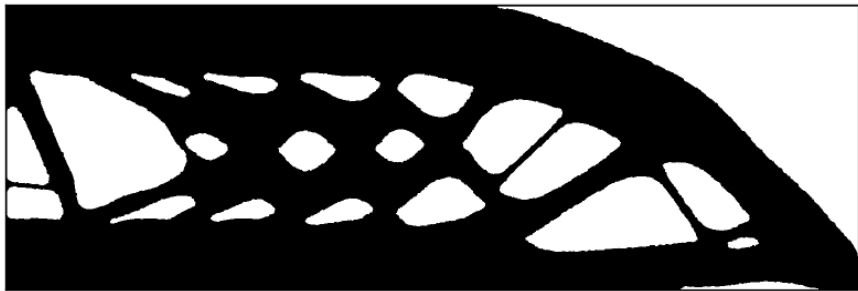


Optimized shape without maximum thickness constraint ($\max d_{\Omega} = 0.36$).

Figure: MBB beam without thickness constraint

Numerical examples

Maximum thickness on MBB beam

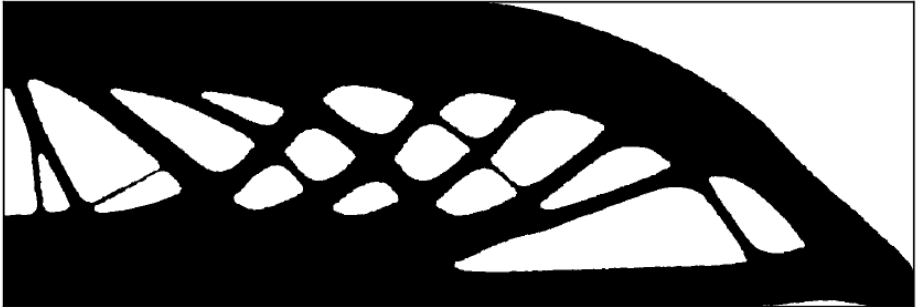


(c) Optimized shape with maximum thickness constraint.

Figure: MBB beam with maximum thickness constraint

Numerical examples

Minimum thickness on MBB beam

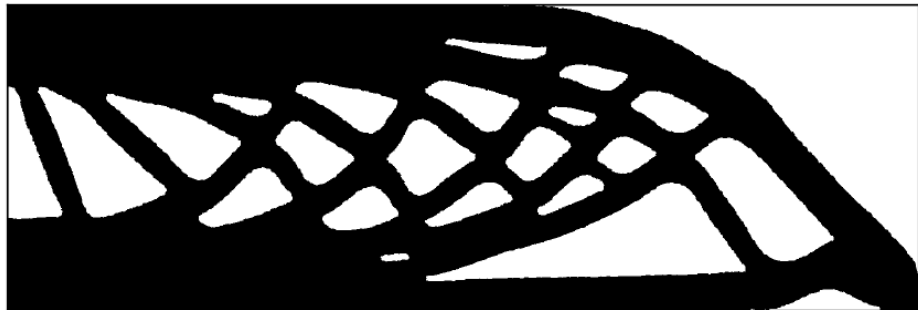


(a) Optimized shape without minimum thickness constraint.

Figure: MBB beam without minimum thickness constraint

Numerical examples

Minimum thickness on MBB beam



(b) Optimized shape with minimum thickness constraint ($d_{\min} = 0.1$).

Figure: MBB beam with thickness constraint

Numerical examples

Minimum thickness on MBB beam

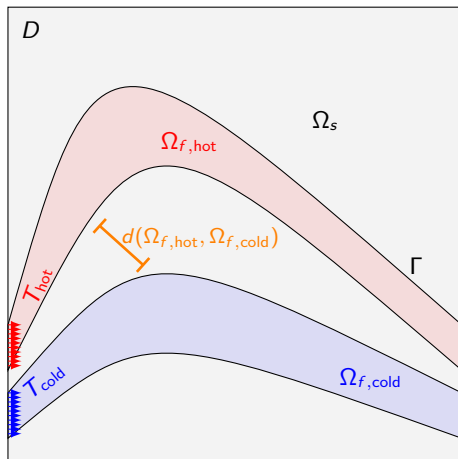


(c) Optimized shape with minimum thickness constraint ($d_{\min} = 0.2$).

Figure: MBB beam with minimum thickness constraint

Numerical examples

Minimum distance constraint



Non-penetration constraint:

$$d(\Omega_{f,hot}, \Omega_{f,cold}) \geq d_{min}.$$

We enforce it by imposing

$$\forall x \in \Omega_{f,cold}, \quad d_{\Omega_{f,hot}}(x) \geq d_{min},$$

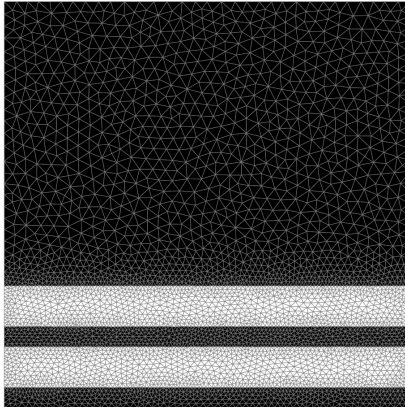
where $d_{\Omega_{f,hot}}$ is the signed distance function to the domain $\Omega_{f,hot}$.

Figure: Settings of the heat exchanger topology optimization problem .

Numerical examples

Minimum distance constraint

Iteration 0



Numerical examples

3D fluid-to-fluid heat exchanger

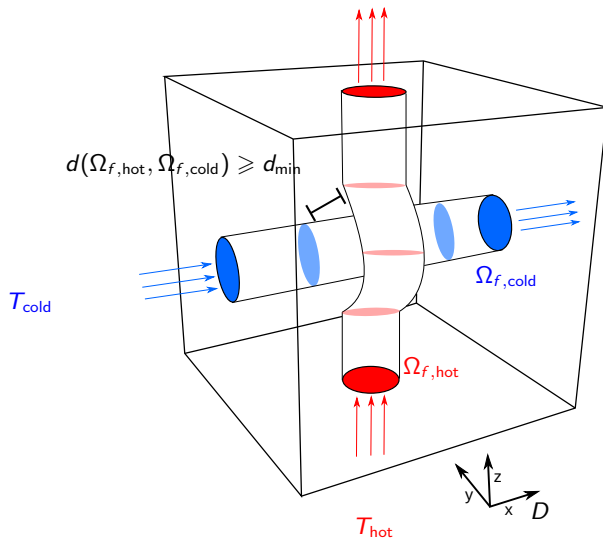


Figure: Schematic of the 3D setting.

Numerical examples

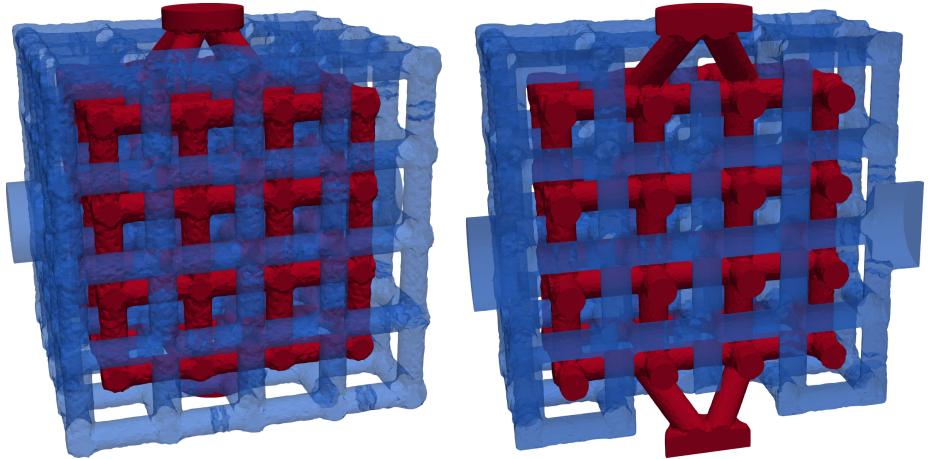
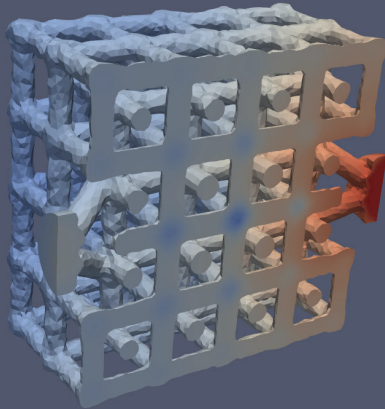
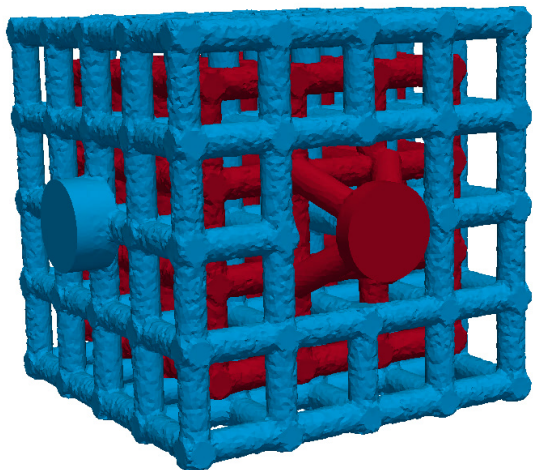


Figure: Initial distribution of fluid considered for the 3D heat exchanger test case.

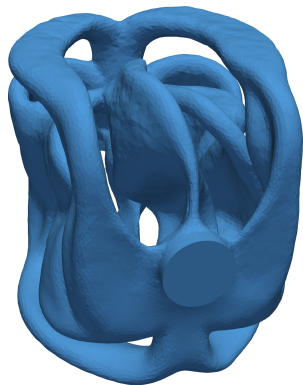
Numerical examples



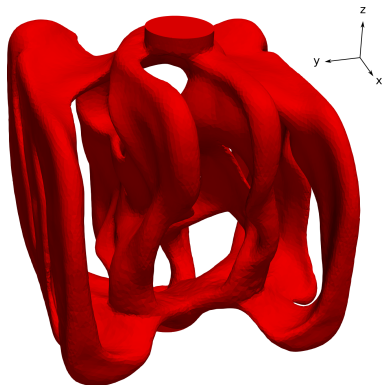
Numerical examples



Numerical examples



(a) Cold phase



(b) Hot phase

Figure: Separate plots of the topologically optimized cold and hot fluid phases in the configuration $d_{\min} = 0.04$.

Numerical examples

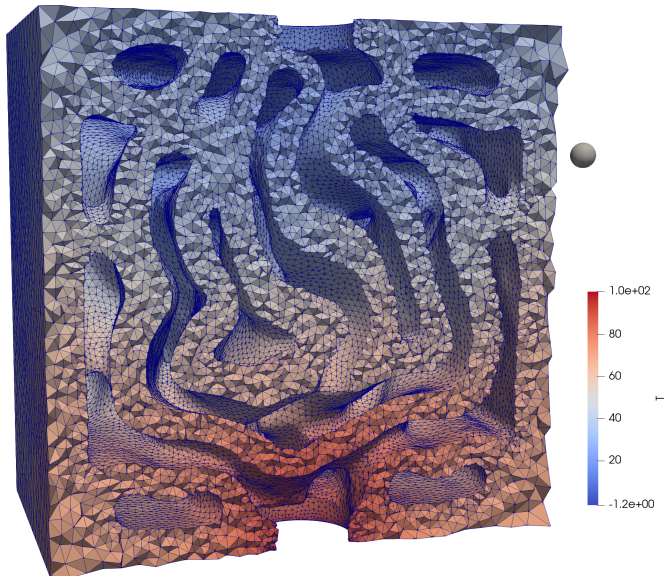


Figure: Cut of the resulting solid domain