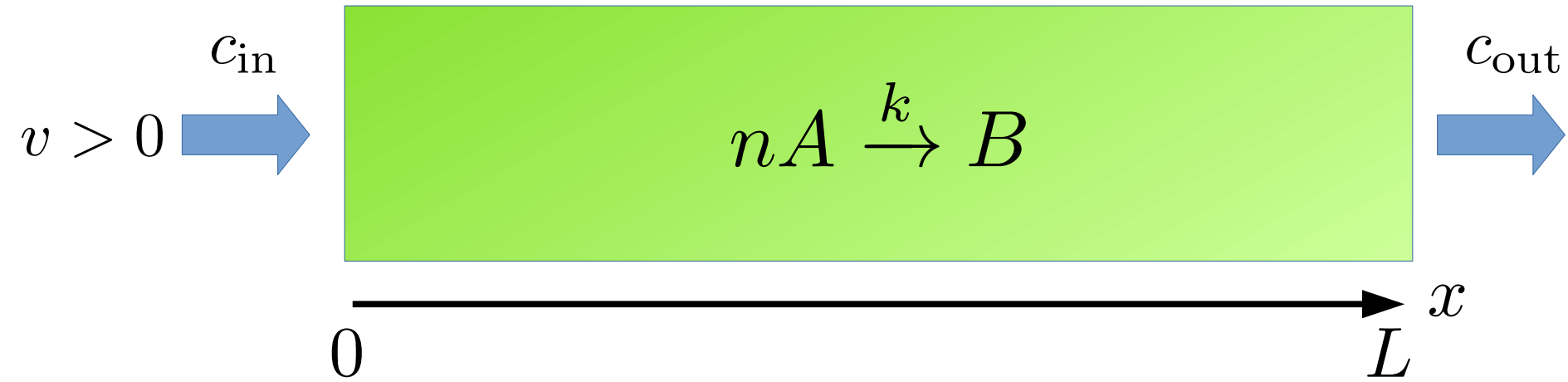


Tubular Reactor



Mass balance:

$$\frac{\partial c}{\partial t} = D \frac{\partial^2 c}{\partial x^2} - v \frac{\partial c}{\partial x} - kc^n$$

Labels for the terms in the mass balance equation:

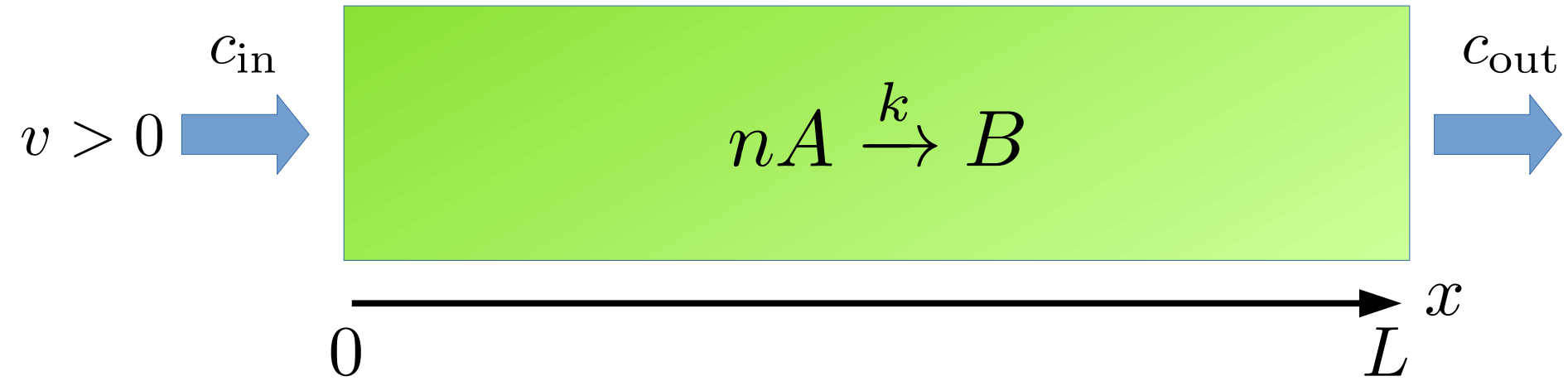
- $D \frac{\partial^2 c}{\partial x^2}$: Diffusion
- $-v \frac{\partial c}{\partial x}$: Advection/Convection
- $-kc^n$: Reaction

Boundary conditions:

$$c(0) - \frac{D}{v} \frac{\partial c}{\partial x}(0) = c_{in} \quad \frac{\partial c}{\partial x}(L) = 0$$

(Danckwerts)

Tubular Reactor



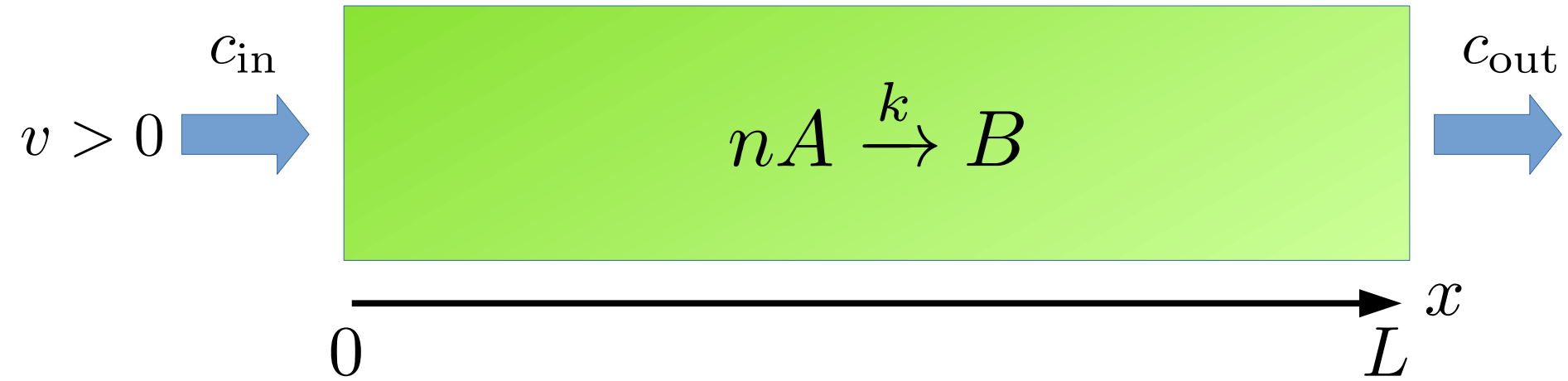
Mass balance:
$$\frac{\partial c}{\partial t} = D \frac{\partial^2 c}{\partial x^2} - v \frac{\partial c}{\partial x} - kc^n$$

Non-dimensionalization:
$$\theta = \frac{t}{\bar{t}} = \frac{tv}{L}$$

$$z = \frac{x}{L}$$

$$u = \frac{c}{c_{in}}$$

Tubular Reactor



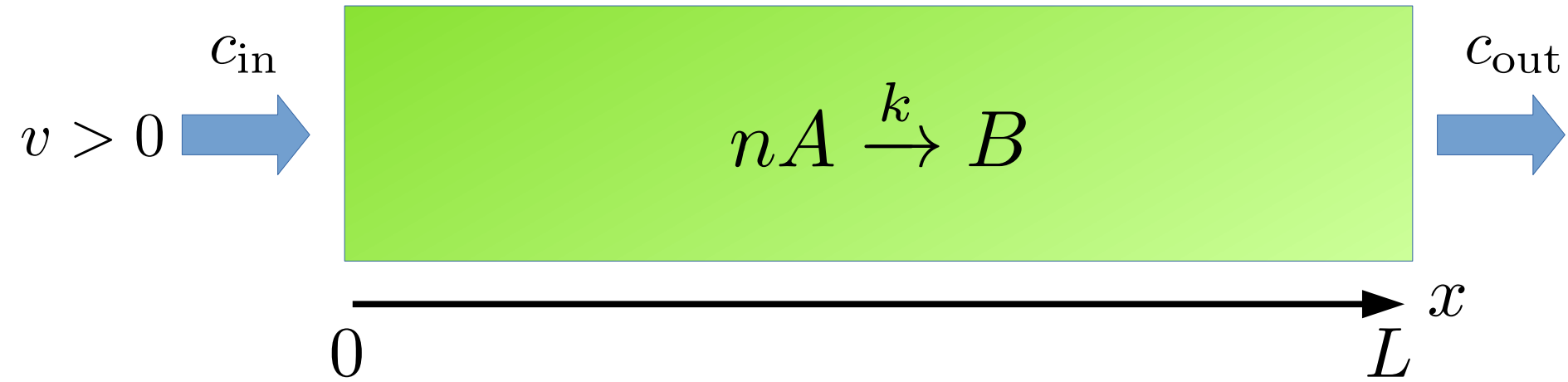
Mass balance:
$$\frac{\partial u}{\partial \theta} = \frac{1}{Pe} \frac{\partial^2 u}{\partial z^2} - \frac{\partial u}{\partial z} - Da \cdot u^n$$

Non-dimensionalization:
$$\theta = \frac{t}{\bar{t}} = \frac{tv}{L}$$

$$z = \frac{x}{L}$$

$$u = \frac{c}{c_{in}}$$

Tubular Reactor

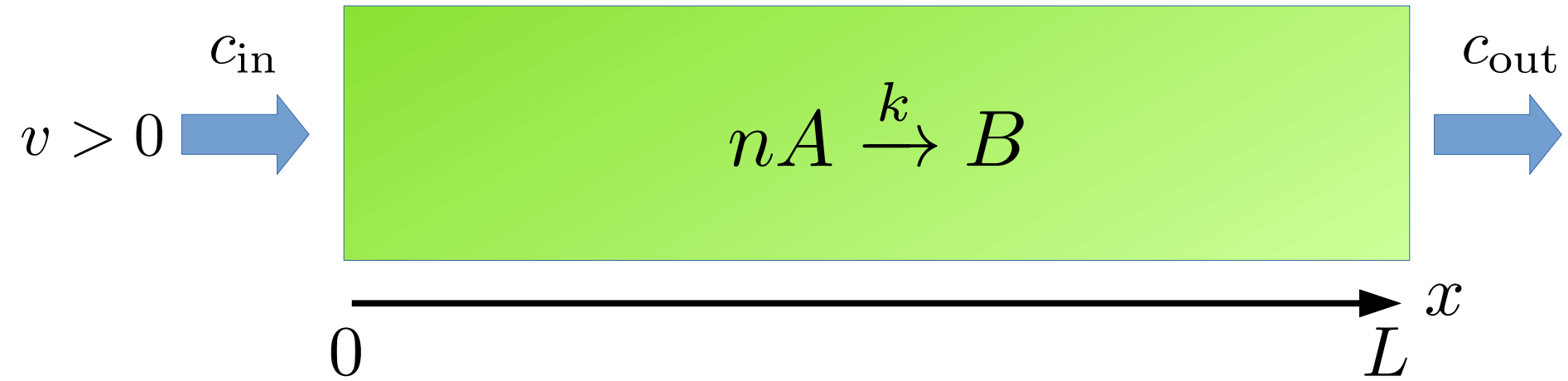


Mass balance:
$$\frac{\partial u}{\partial \theta} = \frac{1}{Pe} \frac{\partial^2 u}{\partial z^2} - \frac{\partial u}{\partial z} - Da \cdot u^n$$

Peclet number:
$$Pe = \frac{L^2/D}{L/v} = \frac{\tau_{Diffusion}}{\tau_{Hydrodynamics}}$$

Damköhler number:
$$Da = \frac{L/v}{1/(kc_0^{n-1})} = \frac{\tau_{Hydrodynamics}}{\tau_{Reaction}}$$

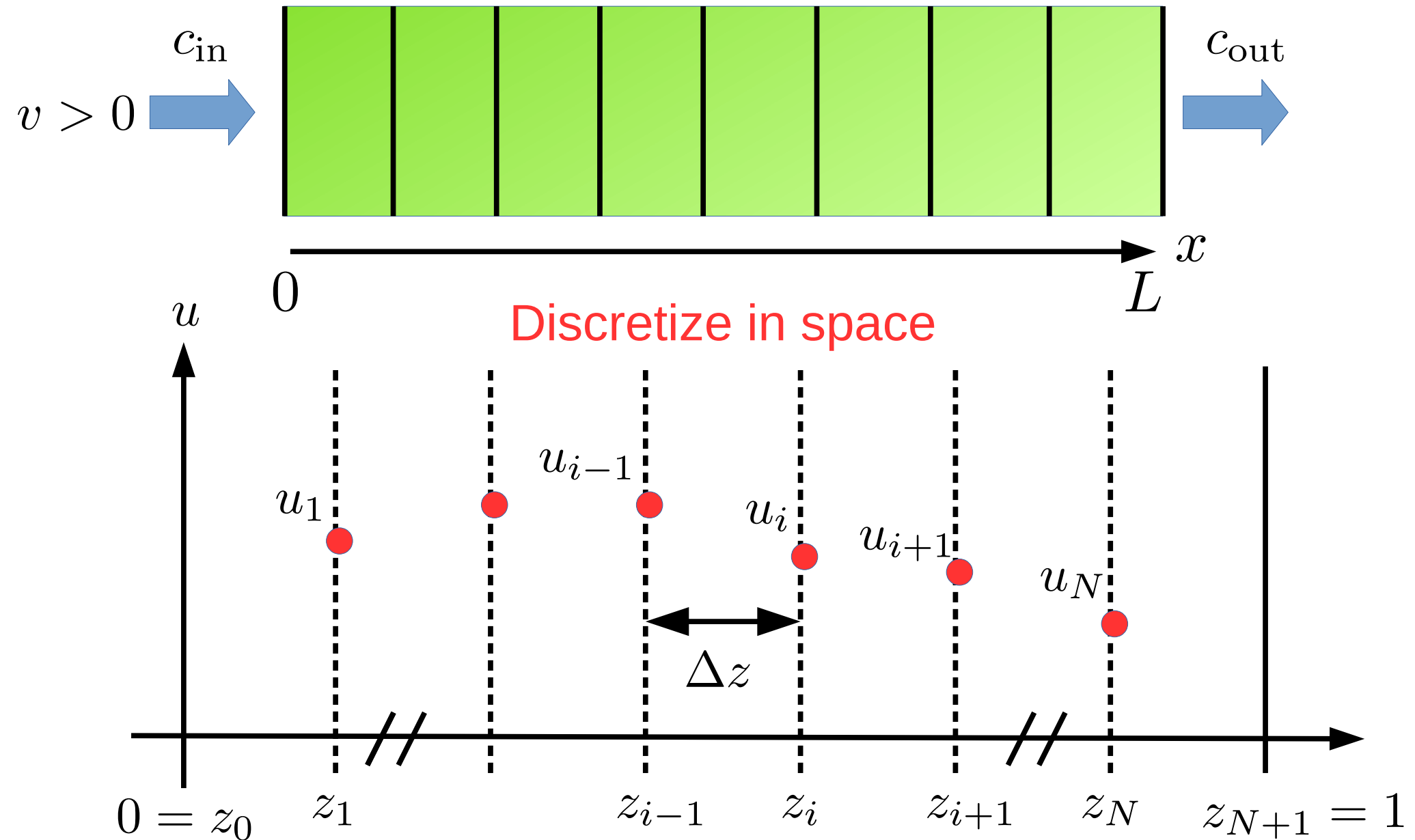
Tubular Reactor



Mass balance:
$$\frac{\partial u}{\partial \theta} = \frac{1}{Pe} \frac{\partial^2 u}{\partial z^2} - \frac{\partial u}{\partial z} - Da \cdot u^n = 0$$

Steady state tubular reactor

Tubular Reactor

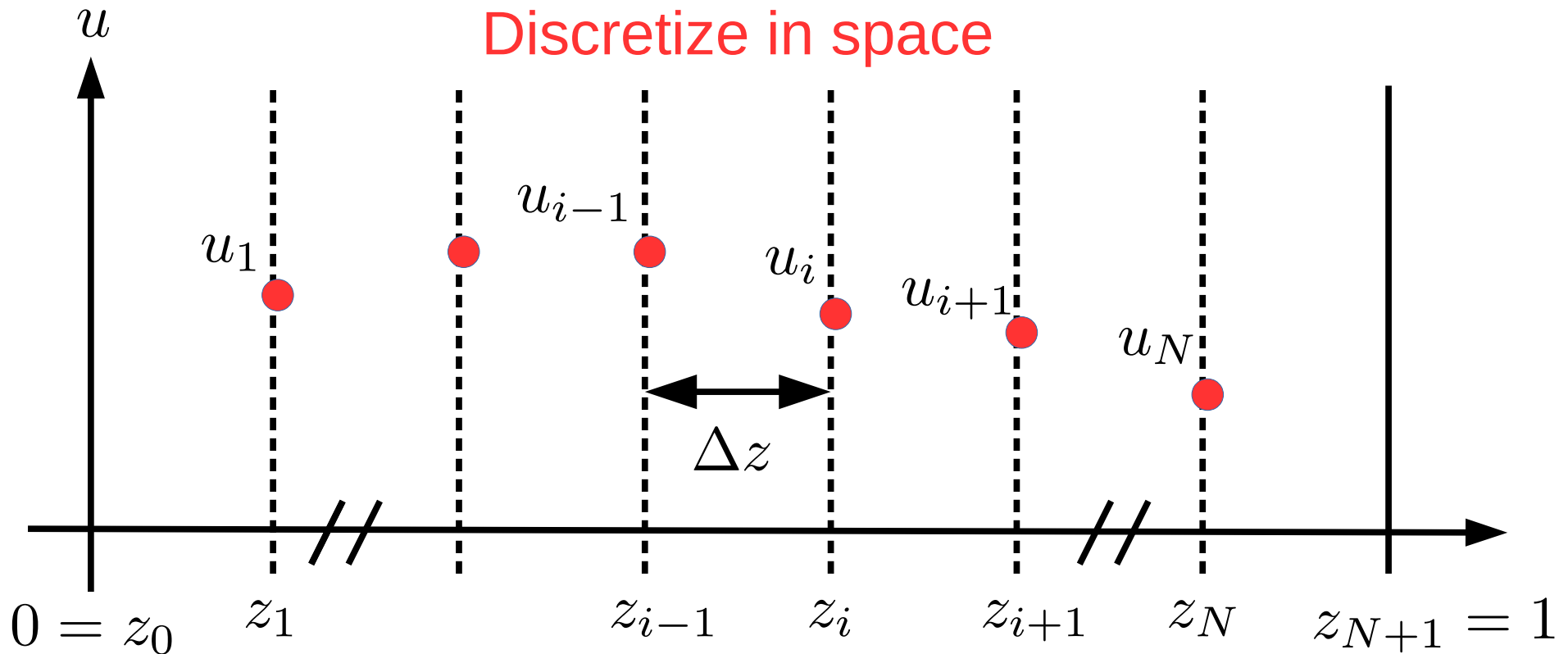


Tubular Reactor

$$\frac{1}{Pe} \frac{\partial^2 u}{\partial z^2} - \frac{\partial u}{\partial z} - Da \cdot u^n = 0$$

$$\frac{1}{Pe} \frac{u_{i+1} - 2u_i + u_{i-1}}{\Delta z^2} - \frac{u_i - u_{i-1}}{\Delta z} - Da \cdot u_i^n = 0$$

Discretize in space



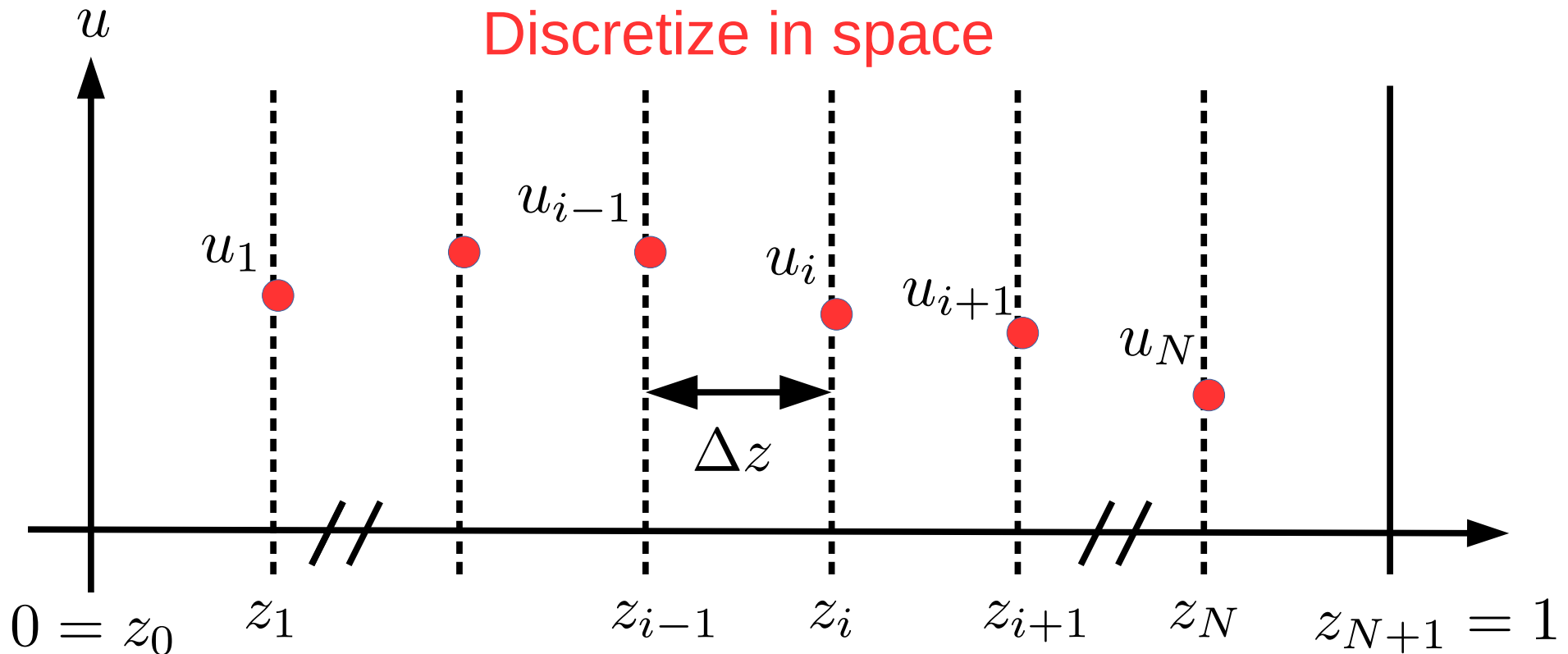
Tubular Reactor

Centered Finite Difference

Backward Finite Difference

$$\frac{1}{Pe} \frac{u_{i+1} - 2u_i + u_{i-1}}{\Delta z^2} - \frac{u_i - u_{i-1}}{\Delta z} - Da \cdot u_i^n = 0$$

Discretize in space

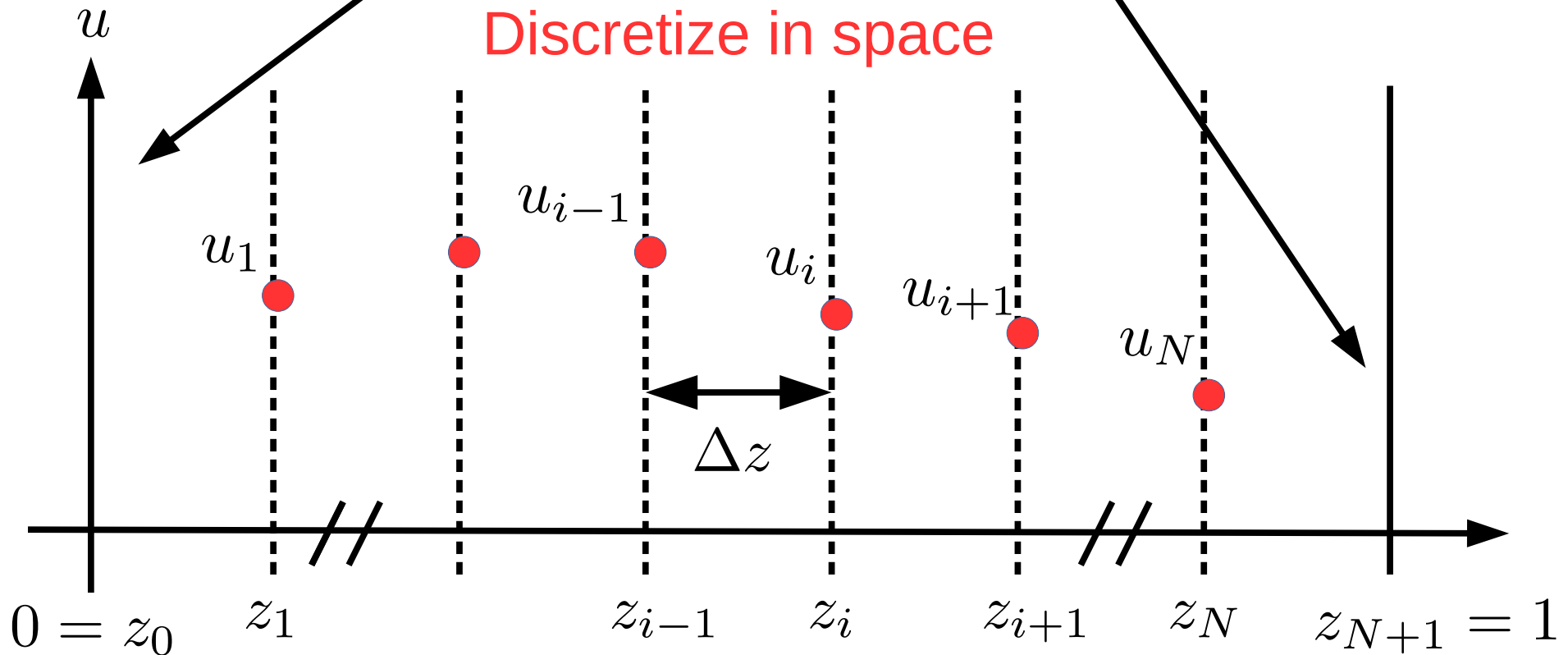


Tubular Reactor

$$\frac{1}{Pe} \frac{u_{i+1} - 2u_i + u_{i-1}}{\Delta z^2} - \frac{u_i - u_{i-1}}{\Delta z} - Da \cdot u_i^n = 0$$

Boundary conditions!

Discretize in space

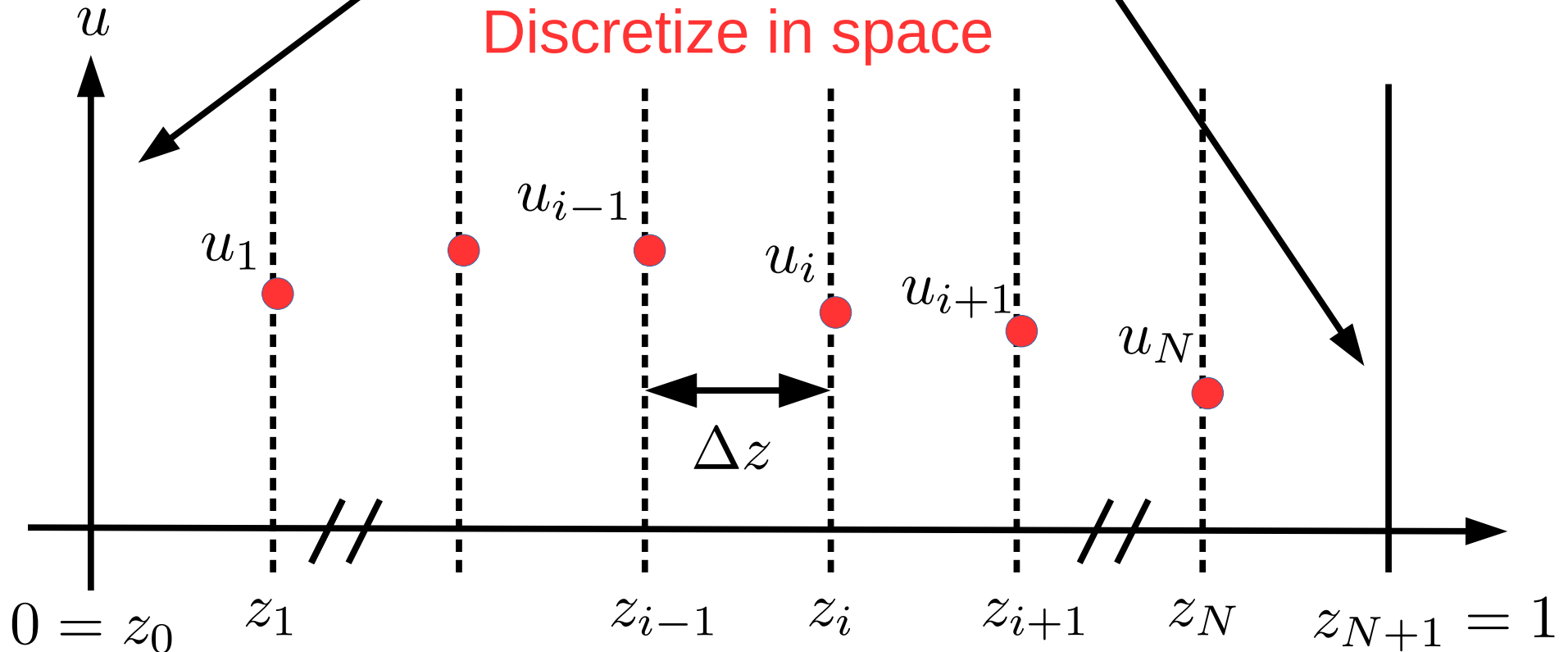


Tubular Reactor

$$\frac{1}{Pe} \frac{u_{i+1} - 2u_i + u_{i-1}}{\Delta z^2} - \frac{u_i - u_{i-1}}{\Delta z} - Da \cdot u_i^n = 0$$

$$u(0) - \frac{1}{Pe} \frac{\partial u}{\partial z}(0) = 1 \quad \frac{\partial u}{\partial z}(1) = 0$$

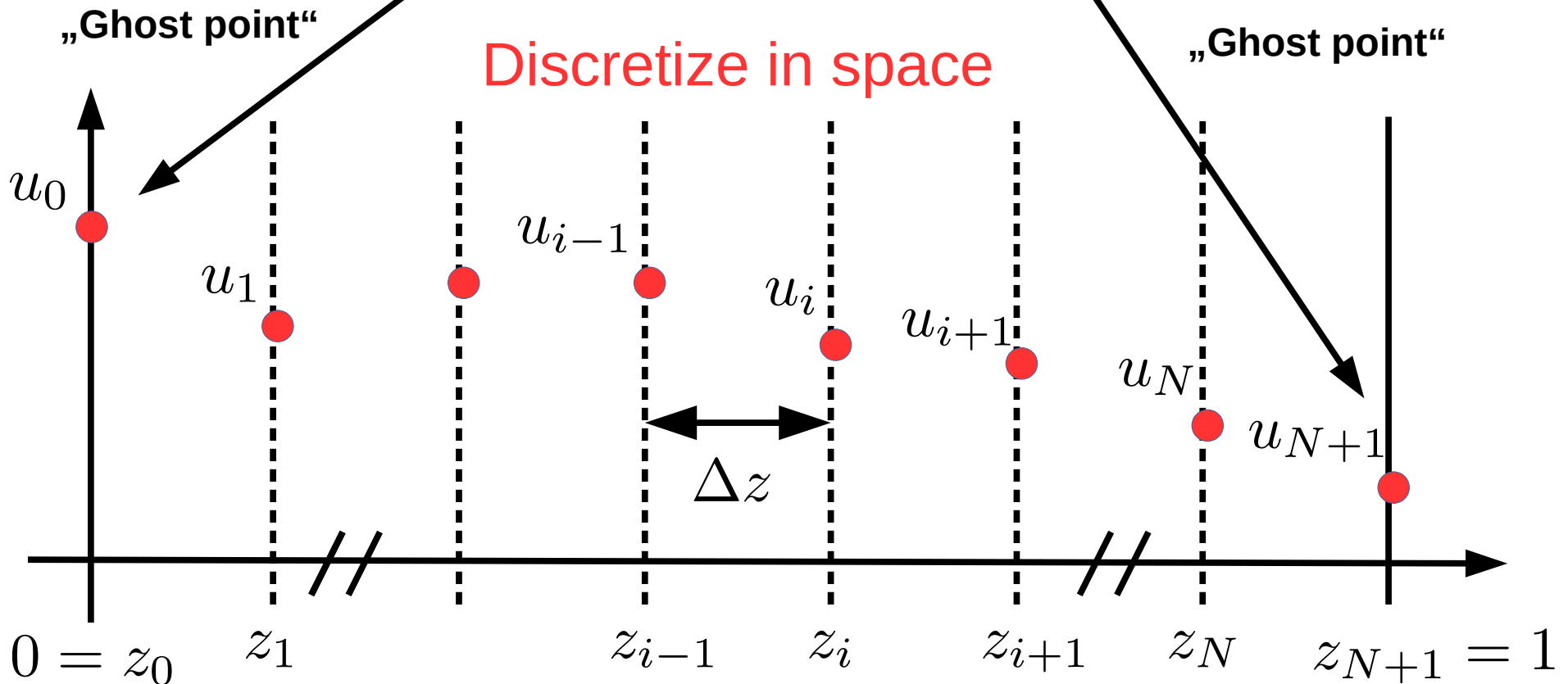
Discretize in space



Tubular Reactor

$$\frac{1}{Pe} \frac{u_{i+1} - 2u_i + u_{i-1}}{\Delta z^2} - \frac{u_i - u_{i-1}}{\Delta z} - Da \cdot u_i^n = 0$$

$$u_0 - \frac{1}{Pe} \frac{u_1 - u_0}{\Delta z} = 1 \quad \frac{u_{N+1} - u_N}{\Delta z} = 0$$



Tubular Reactor

$$\frac{1}{Pe} \frac{u_{i+1} - 2u_i + u_{i-1}}{\Delta z^2} - \frac{u_i - u_{i-1}}{\Delta z} - Da \cdot u_i^n = 0$$

$$u_0 - \frac{1}{Pe} \frac{u_1 - u_0}{\Delta z} = 1 \longrightarrow u_0 = \frac{1}{1 + \frac{1}{Pe\Delta z}} \left(\frac{1}{Pe\Delta z} u_1 + 1 \right)$$

$$\frac{u_{N+1} - u_N}{\Delta z} = 0 \longrightarrow u_{N+1} = u_N$$

$$i = 1, 2, \dots, N$$

System of nonlinear equations!!!

Assignment 1

1. Solve the steady state tubular reactor for 20 different Peclet numbers (between 0.01 and 100) and for a first ($n=1$) and a second ($n=2$) order reaction. Use a Damköhler number of unity.

Complete the template `rhs.m` by implementing the non-linear equations to solve.

2. Plot the conversion at the end of the reactor $1 - \frac{C_{out}}{C_{in}}$ vs. the Peclet number for both reaction orders.

Also plot the ratio between the conversions of the first order and second order reaction

- What is better for these reactions, a lot of back-mixing (Pe small, CSTR) or ideal plug flow (Pe large, PFR)?
- What influence does the reaction order have overall and at low or high Peclet numbers?

Complete the template `TubReact_steady_state.m`

Assignment 1

rhs.m

```
function f = rhs(u,Pe,Da,n);

% function f = rhs(u);
%
% Purpose: compute the right-hand function of the spatially discretized
%          (non-dimensionalized) advection-diffusion-reaction equation for a
%          tubular reactor
%
%           $du/d\theta = - du/dz + 1/Pe d^2u/dz^2 - Da u^n$ 
%
%          using backward finite differences for the advection term and central
%          finite differences for the diffusion term
%
% Input: u ... concentration
%        Pe ... Peclet number
%        Da ... Damkohler number
%        n ... order of reaction
%
% Output: f ... right-hand side function, i.e. du/dtheta
%
% Notes: None.
%

% get number of grid points
N = length(u);

% compute grid spacing \Delta z (since non-dimensionalized 1/(N+1))
dz = 1./(N + 1);

% compute boundary values  $u_{\{0\}}$  and  $u_{\{N+1\}}$ 
Pedz = Pe*dz;
u0 = 0.; % ... COMPLETE HERE ... }
uNp1 = 0.; % ... COMPLETE HERE ... }

% set up u array with boundary values, i.e. "ghost points"
% uGH = [ $u_{\{0\}}$ ,  $u_{\{1\}}$ ,  $u_{\{2\}}$ , ... ,  $u_{\{N-1\}}$ ,  $u_{\{N\}}$ ,  $u_{\{N+1\}}$ ]
uGH = [u0; u; uNp1];

% compute right-hand side function f
f = zeros(size(uGH)); % ... COMPLETE HERE ... }
```

Slide 12

Assignment 1

rhs.m

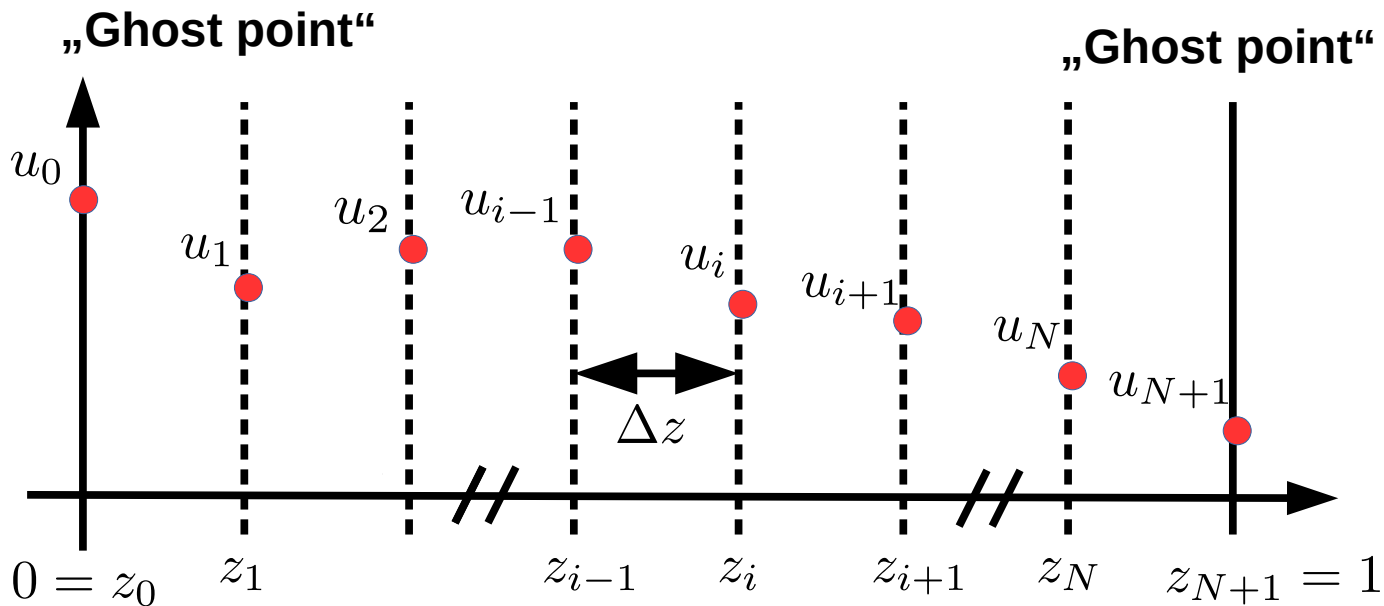
```
function f = rhs(u,Pe,Da,n);
% ...
% get number of grid points
N = length(u);

% compute grid spacing \Delta z (since non-dimensionalized 1/(N+1))
dz = 1./(N + 1);

% compute boundary values u_{0} and u_{N+1}
Pedz = Pe*dz;
u0 = 0.; % ... COMPLETE HERE ...
uNp1 = 0.; % ... COMPLETE HERE ...

% set up u array with boundary values, i.e. "ghost points"
% uGH = [u_{0},u_{1},u_{2}, ... ,u_{N-1},u_{N},u_{N+1}]
uGH = [u0; u; uNp1];

% compute right-hand side function f
f = zeros(size(uGH)); % ... COMPLETE HERE ...
```

$$f_i = \frac{1}{Pe} \frac{u_{i+1} - 2u_i + u_{i-1}}{\Delta z^2} - \frac{u_i - u_{i-1}}{\Delta z} - Da \cdot u_i^n = 0$$


Assignment 1

rhs.m

```
function f = rhs(u, Pe, Da, n);
% ...
% get number of grid points
N = length(u);

% compute grid spacing \Delta z (since non-dimensionalized 1/(N+1))
dz = 1./(N + 1);

% compute boundary values u_{0} and u_{N+1}
Pedz = Pe*dz;
u0 = 0.; % ... COMPLETE HERE ...
uNp1 = 0.; % ... COMPLETE HERE ...

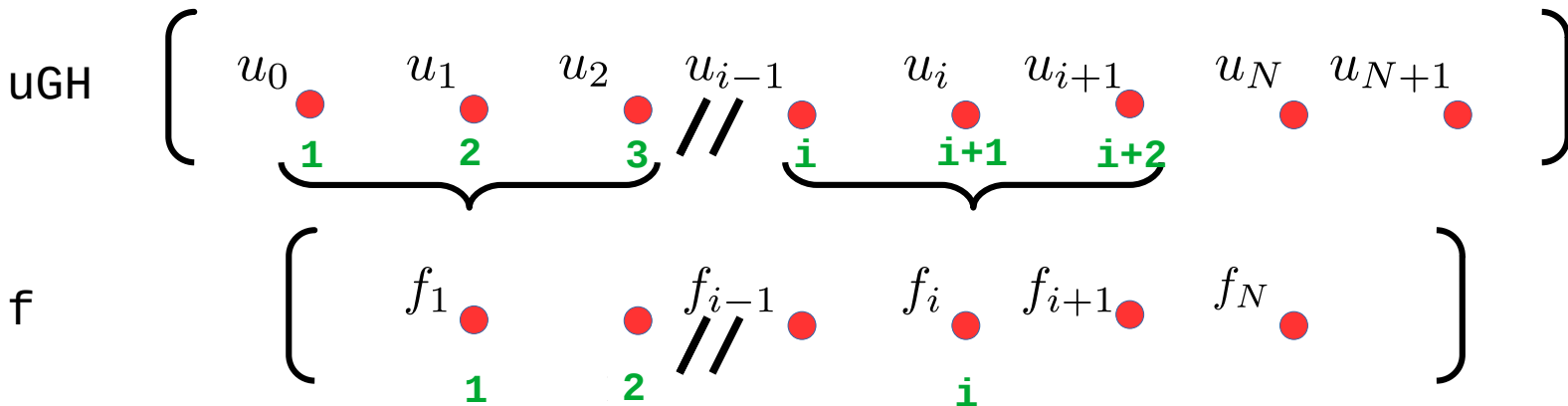
% set up u array with boundary values, i.e. "ghost points"
% uGH = [u_{0}, u_{1}, u_{2}, ... , u_{N-1}, u_{N}, u_{N+1}]
uGH = [u0; u; uNp1];

% compute right-hand side function f
f = zeros(size(uGH)); % ... COMPLETE HERE ...
```

$$f_i = \frac{1}{Pe} \frac{u_{i+1} - 2u_i + u_{i-1}}{\Delta z^2} - \frac{u_i - u_{i-1}}{\Delta z} - Da \cdot u_i^n = 0$$

„Ghost point“

„Ghost point“



Assignment 1

TubReact_steady_state.m

```
% set parameters
N = 100; % number of grid points
NPe = 20; % number of Peclet numbers
Pe = logspace(-2,2,NPe); % generate NPe Peclet numbers log. spaced
    % between 0.01 and 100

Da = 1.; % Damkohler number

% Steady State n = 1 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
n = 1; % reaction order

% allocate array for concentrations
u = zeros(N,1);

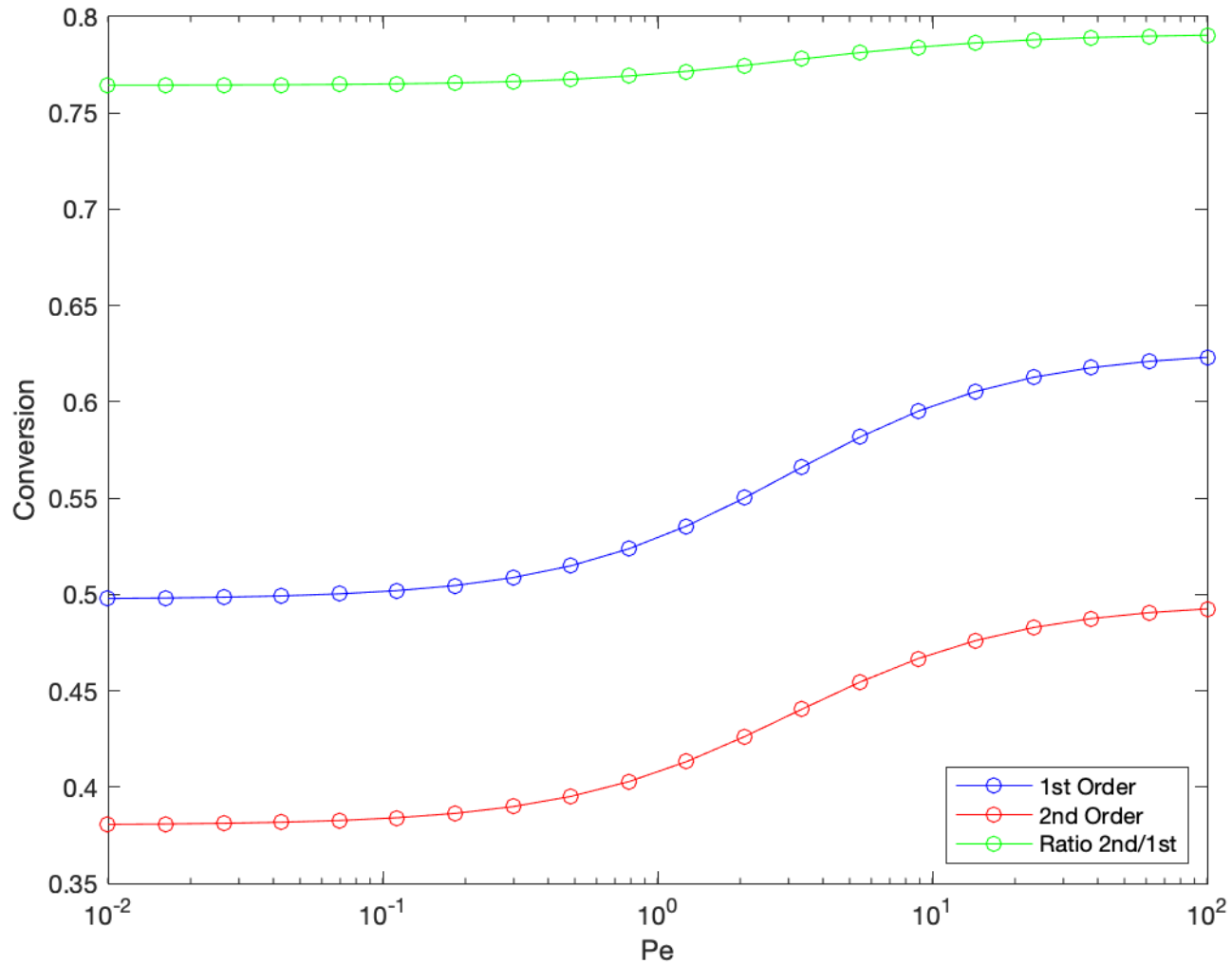
% allocate array for conversion & residuum
Conversion_n1 = zeros(NPe,1);
res_n1 = zeros(NPe,1);

% solve BVP for all desired Peclet numbers
for iPe=1:NPe
    % ... COMPLETE HERE ...
    f = @(u) zeros(length(u),1);
    res_n1(iPe) = norm(f(u),Inf);
end

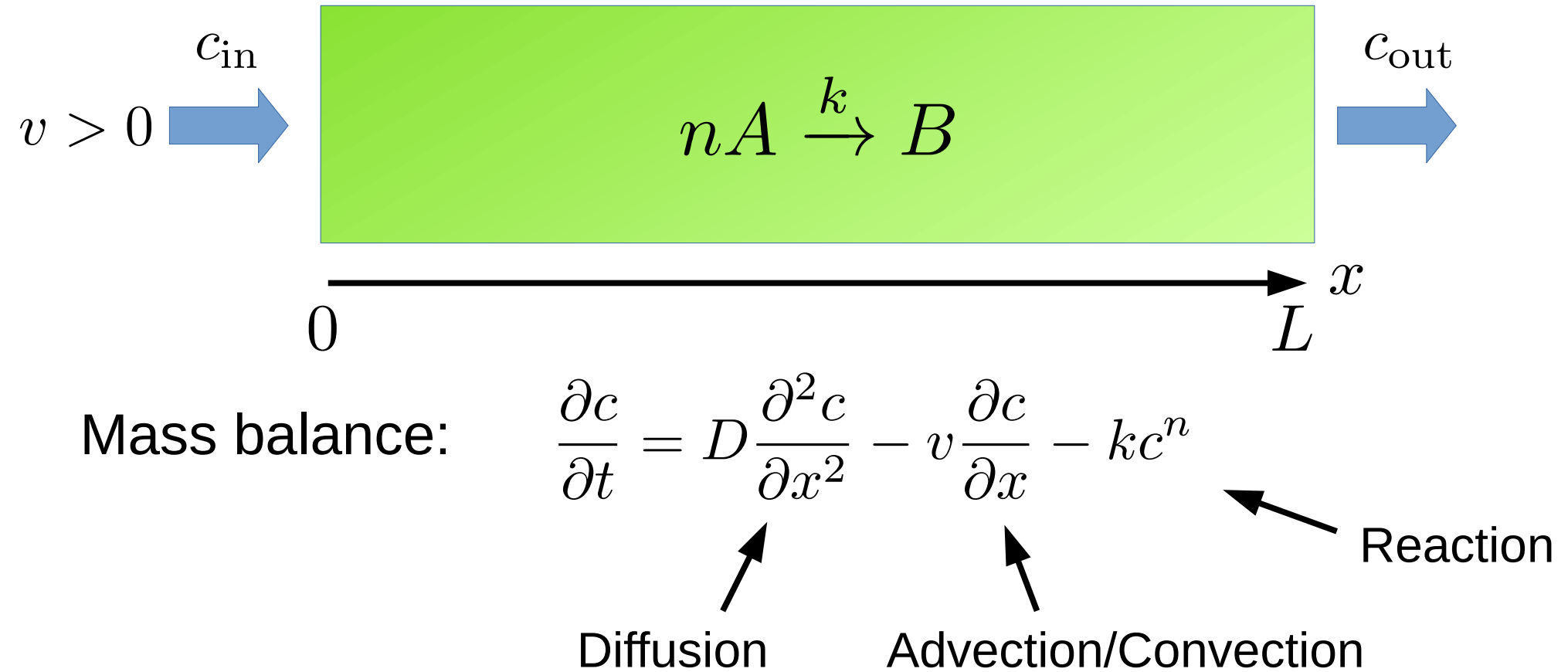
% ...
```

Define a function handle and use fsolve

Assignment 1

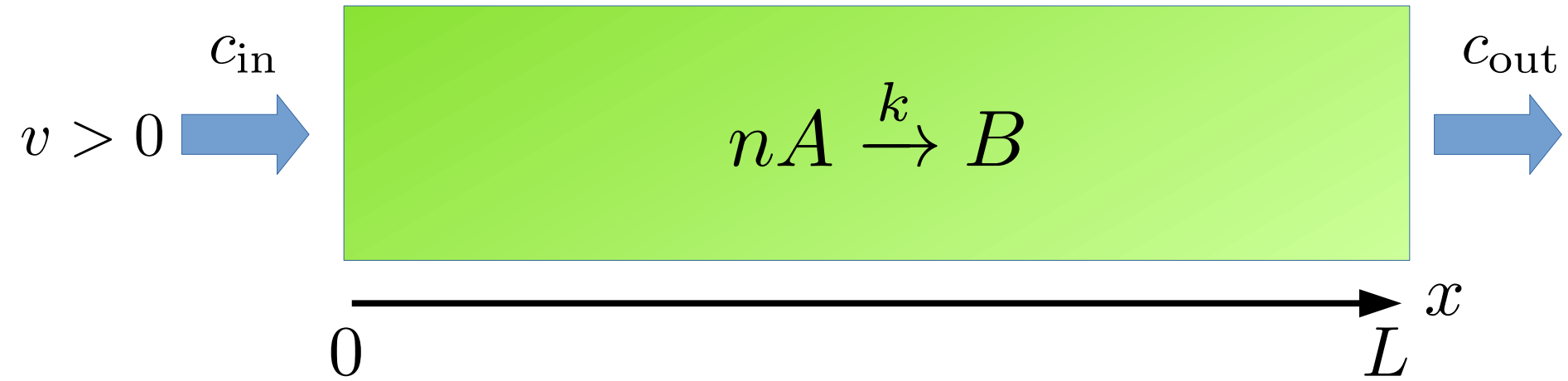


Tubular Reactor



Boundary conditions: $c(0) - \frac{D}{v} \frac{\partial c}{\partial x}(0) = c_{in}$ $\frac{\partial c}{\partial x}(L) = 0$

Tubular Reactor



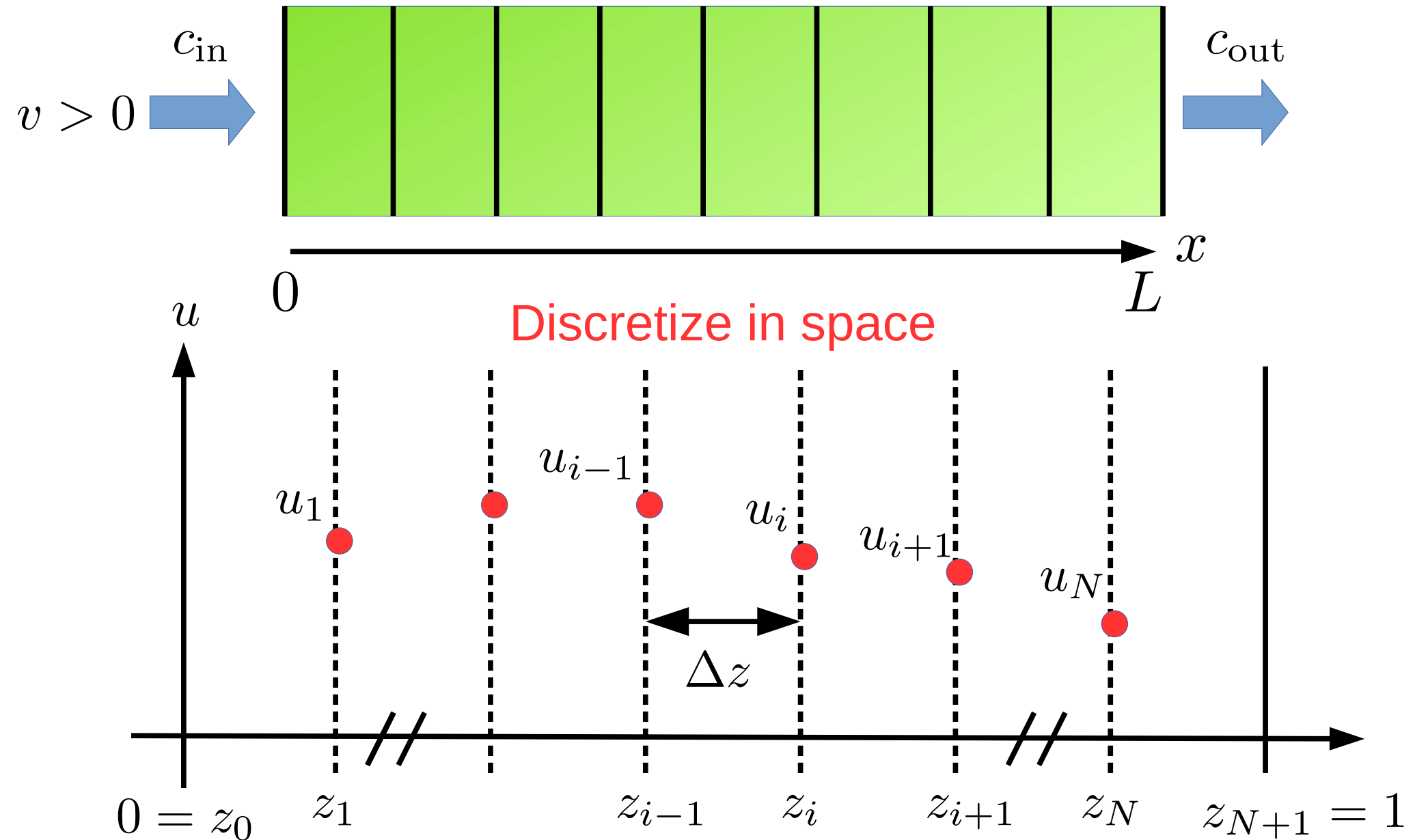
Mass balance:
$$\frac{\partial u}{\partial \theta} = \frac{1}{Pe} \frac{\partial^2 u}{\partial z^2} - \frac{\partial u}{\partial z} - Da \cdot u^n$$

Dynamic tubular reactor

Boundary conditions:

$$u(0) - \frac{1}{Pe} \frac{\partial u}{\partial z}(0) = 1 \quad \frac{\partial u}{\partial z}(1) = 0$$

Tubular Reactor



Tubular Reactor

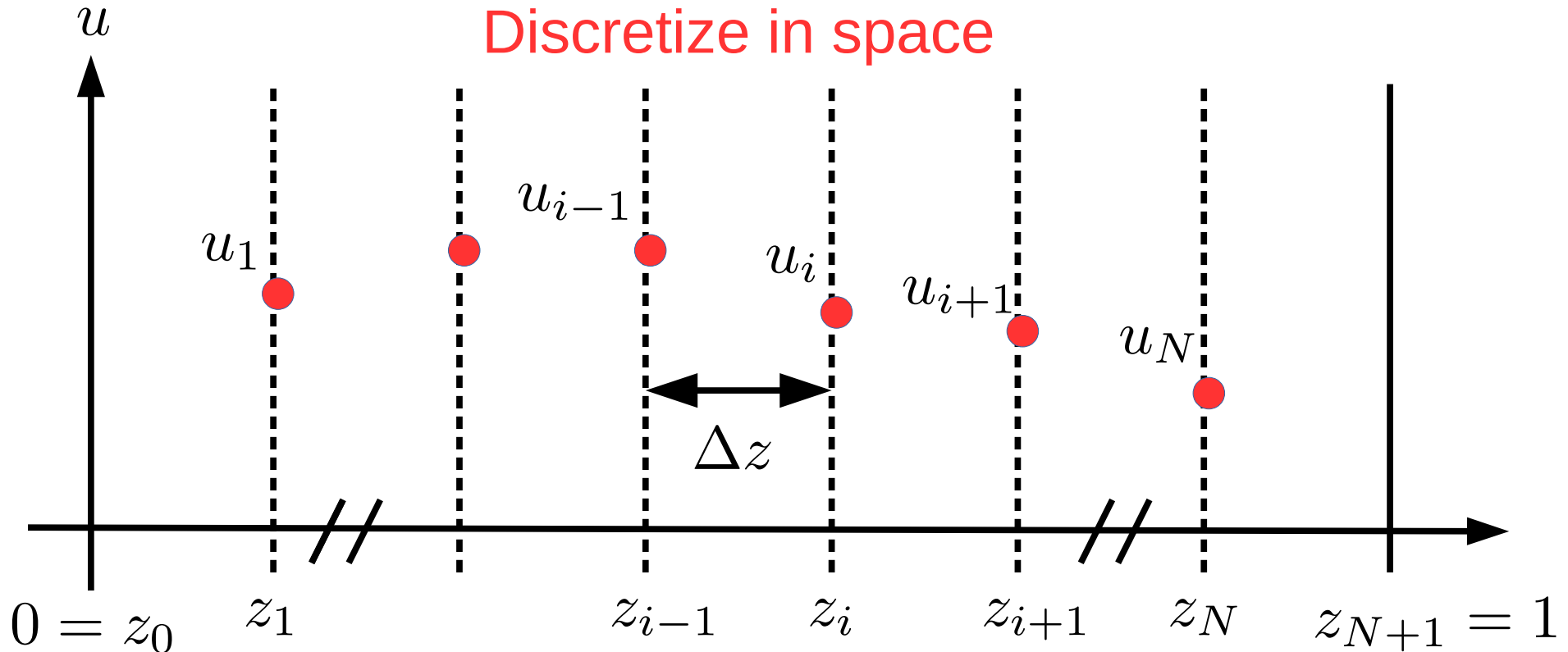
$$\frac{\partial u}{\partial \theta} = \frac{1}{Pe} \frac{\partial^2 u}{\partial z^2} - \frac{\partial u}{\partial z} - Da \cdot u^n$$



ODEs

$$\frac{du_i}{d\theta} = \frac{1}{Pe} \frac{u_{i+1} - 2u_i + u_{i-1}}{\Delta z^2} - \frac{u_i - u_{i-1}}{\Delta z} - k u_i^n$$

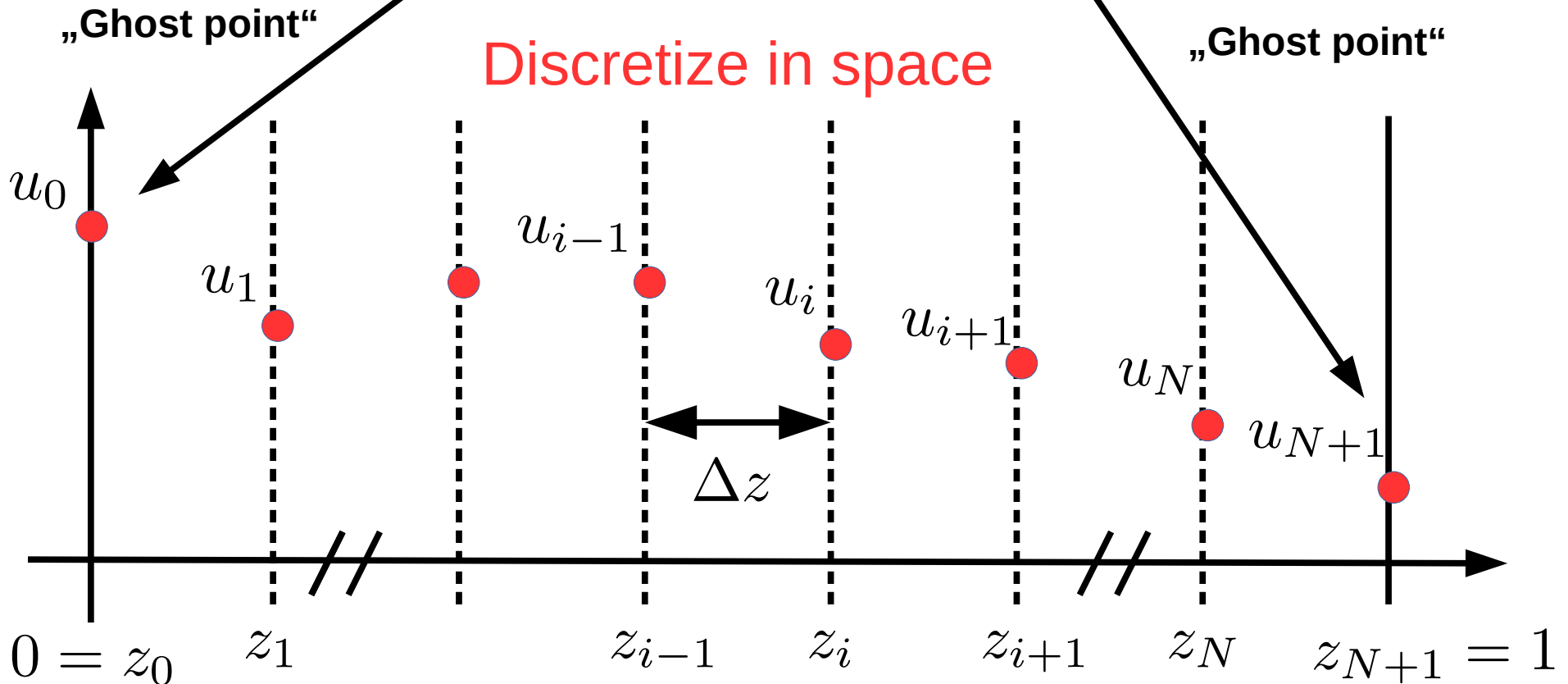
Discretize in space



Tubular Reactor

ODEs
$$\frac{du_i}{d\theta} = \frac{1}{Pe} \frac{u_{i+1} - 2u_i + u_{i-1}}{\Delta z^2} - \frac{u_i - u_{i-1}}{\Delta z} - ku_i^n$$

$$u_0 - \frac{1}{Pe} \frac{u_1 - u_0}{\Delta z} = 1 \quad \frac{u_{N+1} - u_N}{\Delta z} = 0$$



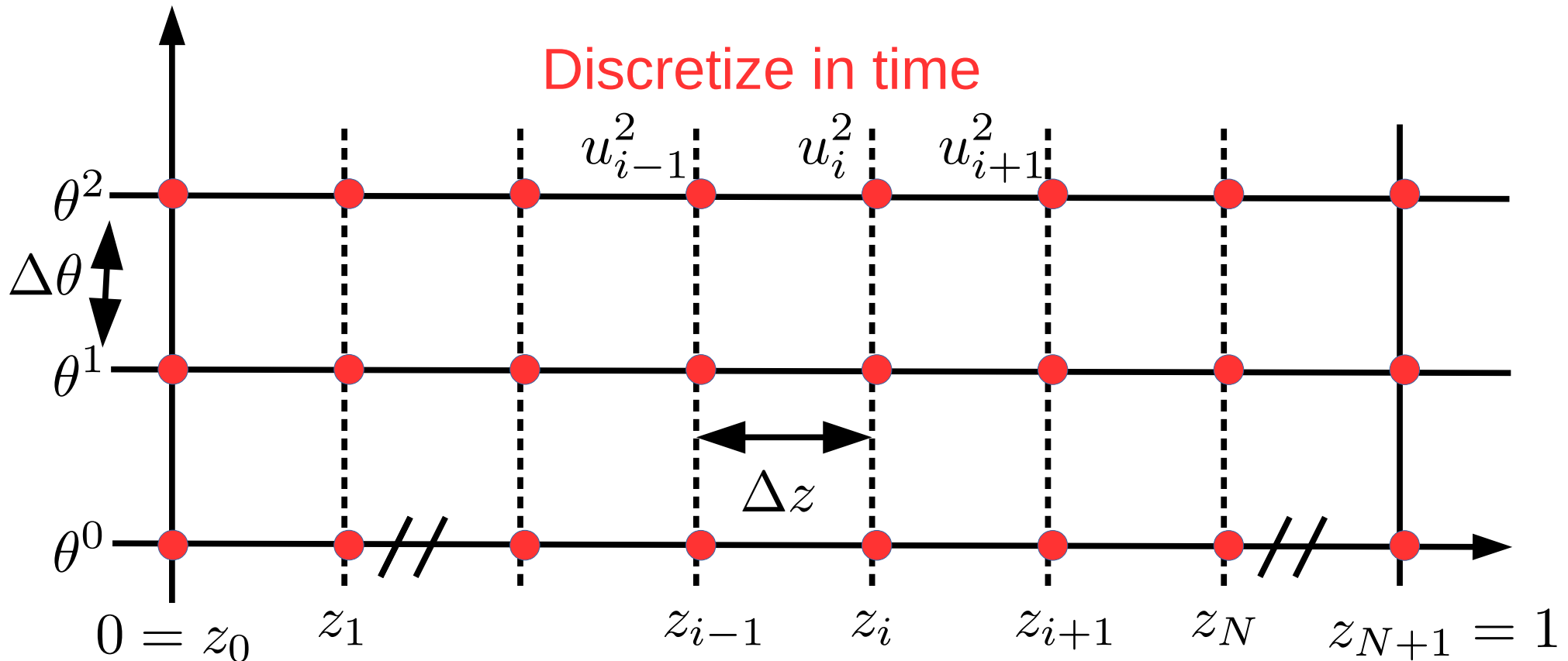
Tubular Reactor

$$\frac{u_i^{n+1} - u_i^n}{\Delta\theta} = \frac{1}{Pe} \frac{u_{i+1}^n - 2u_i^n + u_{i-1}^n}{\Delta z^2} - \frac{u_i^n - u_{i-1}^n}{\Delta z} - k(u_i^n)^{\tilde{n}}$$

Time index
Order of reaction

t

E.g. Explicit Euler, ... But in general ver stiff



Tubular Reactor

$$\frac{du_i}{d\theta} = \frac{1}{Pe} \frac{u_{i+1} - 2u_i + u_{i-1}}{\Delta z^2} - \frac{u_i - u_{i-1}}{\Delta z} - ku_i^n$$

$$u_0 - \frac{1}{Pe} \frac{u_1 - u_0}{\Delta z} = 1 \longrightarrow u_0 = \frac{1}{1 + \frac{1}{Pe\Delta z}} \left(\frac{1}{Pe\Delta z} u_1 + 1 \right)$$

$$\frac{u_{N+1} - u_N}{\Delta z} = 0 \longrightarrow u_{N+1} = u_N$$

$$i = 1, 2, \dots, N$$

System of nonlinear ODEs!!!
Stiff...

Assignment 2

1. Solve the dynamic tubular reactor from initial 0 to final time of 5 with MATLAB's `ode23s`
Use the `rhs.m` from assignment 1 and the template `TubReact_dynamic.m`
Consider only a first order reaction with $Pe=100$ and $Da=1$
2. Plot the conversion at the end of the reactor vs. dimensionless time
3. At what time does the solution reach a steady state, i.e. how many reactor volumes of solvent will you need?

Assignment 2

